# TRIBUTE (BROOKDALE) LIMITED

1101A, 1105, and 1163 Kingston Road

October 27, 2023



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# 1101A, 1105 AND 1163 KINGSTON ROAD FUNCTIONAL SERVICING REPORT

TRIBUTE (BROOKDALE) LIMITED

FUNCTIONAL SERVICING REPORT

PROJECT NO.: 221-12931 DATE: OCTOBER 2023

WSP CANADA INC. 100 COMMERCE VALLEY DRIVE WEST THORNHILL, ON, CANADA L3T 0A1

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# **1** INTRODUCTION

WSP has been retained by Tribute (Brookdale) Limited to prepare a Functional Servicing Report in support of the proposed redevelopment of the site located at 1101A, 1105 and 1163 Kingston Road in the City of Pickering, Ontario. The proposed plan, which will be constructed in four phases, involves the redevelopment of the existing commercial site into a six building multi-use development. This report provides the conceptual framework for water distribution, sanitary sewage and storm drainage for the site prior to the commencement of detailed design. A Stormwater Management Report outlining the proposed conceptual Stormwater Management controls on this site has been prepared by WSP under a separate cover.

In preparing this report, WSP staff secured and reviewed the Site Plan prepared by Turner Fleischer Architects Inc. dated October 23, 2023, topographic surveys prepared by J.D. Barnes Ltd. dated February 2, 2023 (see **Appendix E**), and record drawings provided by the Region of Durham (see **Appendix E**). This report is intended to provide the functional design framework for the proposed development. All required approvals from the City of Pickering, Region of Durham, and all other governing bodies shall be obtained as part of the registration of the development.

## 1.1 SITE DESCRIPTION

The subject site is approximately 7.75 ha (19.15 acres), and it is located at 1101A, 1105 and 1163 Kingston Road in the City of Pickering, Ontario. The site is bounded by Kingston Road to the north-west, a segment of Walnut Lane and a segment of Public Road to the north-east, Highway 401 to the south and existing commercial lands to the west. Under the existing conditions, the site contains five commercial buildings. The location and existing site conditions are illustrated in **Figure 1-A – "Location Map"**, and **Figure 1-B – "Pre-development Plan"** respectively.

Based on the site plan provided by Turner Fleischer, the proposed development will be mixed use, and it will include six buildings that will be constructed across four phases. The intention of the phasing is to keep the existing commercial developments located outside of the phase limits operational in the interim condition. The existing public driveway that runs along the north-east boundary of the site will also be replaced by a complete 20.0 m R.O.W. as part of the Walnut Lane extension project.

The first phase, which will be located at the north end of the development will introduce two new buildings (Buildings 'A1' and 'A2') that will fall under the same condo corporation. With the introduction of these buildings, three of the existing commercial developments located within the site will be removed. The second phase, which will be located at the south-east corner of the site, will introduce one new Building (Building 'B') and one existing commercial development will be removed. The third phase, which will be located in the middle of the site, will introduce two new buildings (Buildings 'C1' and 'C2') that will fall under the same condo corporation. No existing commercial developments will be removed in Phase 3. The fourth phase will introduce one new Building (Building 'D') and one existing commercial development will be removed.

The development statistics that summarize each of the proposed phases are outlined in Table 1. The ultimate conditions are illustrated in **Figure 1-C - "Post Development Plan"**.

Phase	Area (ha)	Building	Land Use	Units	Residential Population	Commercial GFA (sq.m.)	Number of Floors	
1	1.76	Building 'Al'	Mixed-Use Residential	609	1,214	4,946	19+MPH	
		Building 'A2'	Mixed-Use Residential	602	1,199	716	23+MPH	
2	1.61	Building 'B'	Residential	1,303	2,593	N/A	35+MPH	
3	1.91	Building 'Cl'	Mixed-Use Residential	1,103 <sup>(1)</sup>	2,195	2203	27+MPH	
		Building 'C2'	Residential				N/A	27+MPH
4	2.47	Building 'D'	Residential	1,621	3,226	N/A	35+MPH	
TOTAL	7.75			5,238	10,427	4,865		

Table 1 - Development Statistics Summary

<sup>(1)</sup> At the time of writing this report the delineation of the total unit count across the proposed buildings had not yet been determined.

<sup>(2)</sup> Occupancy rates, per capita flows and peaking factor are as per the Region of Durham Design Specifications

<sup>(3)</sup> Unit Counts and Floor Areas from drawings prepared by Turner Fleisher, dated October 23, 2023

### 1.2 PUBLIC RIGHT - OF - WAY

A municipal road that runs through the site and connects to Walnut Lane is proposed as part of the site plan. The road will run in a north-south direction on the west side of the Phase 2 lands, and it will run in the east - west direction on the south side of the Phase 3 lands. The public road will terminate at the west property boundary, with the option to extend this road to Dixie Road in the future. The proposed municipal right - of - way will be 20.0 m in size, and it will contain an 8.5 m pavement width and boulevard areas on each side. The proposed road layout is outlined in **Figure 1-C – "Post Development Plan".** 







# 2 WATER SUPPLY AND APPURTENANCES

## 2.1 EXISTING CONDITIONS

Based on the record drawings from the Region of Durham, and the topographic surveys prepared by J.D. Barnes Ltd the existing infrastructure in the vicinity of the site is as follows:

- > a 300 mm diameter watermain on Kingston Road north of the site;
- a 250 mm diameter watermain on Walnut Lane;
- a 100 mm diameter watermain on Walnut Lane;
- a series of 100 250 mm diameter watermains located within the existing commercial site that service the existing commercial developments; and
- an external chamber and backflow preventor room located east of Walnut Lane that services all buildings within the existing development.

The location of the existing water services is illustrated in Figure 2A - "Existing Watermains".

## 2.2 MUNICIPAL WATERMAIN IMPROVEMENTS

A new 300 mm diameter watermain will be constructed north of the site as part of the future Walnut Lane extension. The proposed watermain will connect to the existing watermains on Liverpool Road and Kingston Road. The future watermain will be active at the time of the proposed redevelopment of this site, so the intention is to use it as the connection point for the proposed development. At this time, it is WSP's understanding that the 300 mm diameter watermain will have the capacity to service the proposed development.

## 2.3 PROPOSED WATER SERVICES

An illustration of the proposed water servicing strategy for each phase is outlined in **Figures 2B - 2E**. The following subsections describe the proposed water servicing in detail.

#### 2.3.1 PHASE 1

In Phase 1, a set of domestic and fire water service connections will be made directly to the future watermain on Walnut Lane to service Buildings 'A1' and 'A2'. The connections will be made in accordance with Region of Durham Standards. If the height of these towers exceeds 84 m, a secondary fire connection will be provided as per Ontario's building code requirements. Sizing of the

water service connections will be coordinated with the Region of Durham and the mechanical engineering consultant at the detailed design stage.

To limit the disturbance to the existing commercial development during the construction of Phase 1, all watermains intersecting the Phase 1 limits will be capped at the phase limit. Since none of the existing buildings relying on these watermains will be preserved during Phase 1, no temporary water servicing strategy will be required. Refer to **Figure 2B** - **"Phase 1 Water Servicing"** for an illustration of the proposed water servicing strategy for Phase 1.

#### 2.3.2 PHASE 2

In Phase 2, a 300 mm diameter watermain will be installed within the proposed 20.0 m R.O.W west of Building 'B'. The proposed 300 mm diameter watermain will connect to the future watermain in Walnut Lane, and it will be used to service the domestic and fire connections for Building 'B'. The water connections for Building 'B' will be made in accordance with Region of Durham Standards, and if the height of these towers exceeds 84 m, a secondary fire connection will be provided as per Ontario's building code requirements. Sizing of the water service connections will be coordinated with the Region of Durham and the mechanical engineering consultant at the detailed design stage.

According to the topographic surveys prepared by J.D. Barnes Ltd, the existing commercial development in the south of the site has water connections that fall within the west limits of Phase 2. These connections will have to be removed to accommodate the underground structure of Building 'B', so temporary domestic and water service connections will have to be installed to re-route these existing services outside of the proposed underground structure. The temporary connections will connect to the proposed 300 mm watermain installed within the proposed R.O.W introduced in Phase 2 to prevent additional disruption to the existing development. Since the existing building relies on an external chamber and backflow preventor room located within the Phase 3 lands, a temporary chamber and backflow preventor room are proposed to be installed to service the existing building in the interim condition.

Refer to **Figure 2C - "Phase 2 Water Servicing"** for an illustration of the proposed water servicing strategy for Phase 2.

#### 2.3.3 PHASE 3

In Phase 3, the proposed 300 mm diameter watermain from Phase 2 will be extended west across the proposed R.O.W extension. The watermain will be capped at the property line on the west side of the site. Extending the watermain enables future connection if the R.O.W is ultimately extended to Dixie Road.

To service Buildings 'C1' and 'C2', a set of domestic and fire water service connections will be made to the proposed 300 mm diameter watermain within the 20.0 m R.O.W. The connections will be made in accordance with Region of Durham Standards, and if the height of the buildings exceeds 84 m, a secondary fire connection will be provided as per Ontario's building code requirements. Sizing of the

water service connections will be coordinated with the Region of Durham and the mechanical engineering consultant at the detailed design stage.

Refer to **Figure 2D - "Phase 3 Water Servicing"** for an illustration of the proposed water servicing strategy for Phase 3.

#### 2.3.4 PHASE 4

In Phase 4, Building 'D' will have domestic and fire water service connections to the proposed 300 mm diameter watermain within the 20.0 m R.O.W north of the building. The water connections for Building 'D' will be made in accordance with Region of Durham Standards, and if the height of these towers exceeds 84 m, a secondary fire connection will be provided as per Ontario's building code requirements. Sizing of the water service connections will be coordinated with the Region of Durham and the mechanical engineering consultant at the detailed design stage. Refer to **Figure 2E - "Phase 4 Water Servicing"** for an illustration of the proposed water servicing strategy for Phase 4.











# **3 SANITARY SEWAGE SYSTEM**

## 3.1 EXISTING CONDITIONS

Based on the record drawings from the Region of Durham, and the topographic surveys prepared by J.D. Barnes Ltd the existing infrastructure in the vicinity of the site is as follows:

- 1050 mm diameter trunk sanitary sewer on the south side of the site;
- > 200 mm diameter sanitary sewers located in an easement on the west side of the site;
- > 200 mm diameter sanitary sewer on Walnut Lane; and
- > 200 mm diameter sanitary sewer north of the site on Kingston Road.

In the existing condition, all sanitary waste generated within the site is ultimately discharged to the 1050 mm diameter trunk sewer. The methods of connection to the trunk are summarized below:

- > The two buildings on the south side of the site have direct connections to the trunk;
- The building on the west side of the site is conveyed to the trunk via the 200 mm diameter sanitary sewer located in the easement on the west side of the site; and
- The two buildings on the north side of the site have connections to the Kingston Road sanitary sewer before connecting to the 1050 mm diameter trunk sewer.

Figure 3A - "Existing Sanitary Sewers" illustrates the existing on - site sanitary servicing strategy.

## 3.2 DESIGN PARAMETERS

To calculate the peak sanitary flows, the following Region of Durham design criteria has been utilized:

- ▶ 180,000 L / ha / day average day flow generation rate for commercial use;
- 364 L / cap / day average day flow generation rate for residential use;
- Population equivalent based on unit type for residential use:
  - o 1.5 people per one Bedroom residential apartment unit;
  - o 2.5 people per two Bedroom residential apartment unit;
  - o 3.5 people per three Bedroom residential apartment unit; and
  - o 4.5 people per four Bedroom residential apartment unit.
- Peaking Factor for residential use: Harmon Formula  $KH = 1 + \frac{14}{4+P^{0.5}}$ ; and
- ▶ Infiltration: 0.26 L / ha / s.

## 3.3 POST - DEVELOPMENT SEWAGE FLOW

The anticipated post - development sanitary flows to the downstream sanitary sewer system have been calculated based on the Region of Durham Design Criteria and site statistics provided by Turner Fleischer Architects Inc. dated October 23, 2023. Detailed flow generation design sheets are included in **Appendix A**. The flow summary for each phase is included in **Table 2**.

Phase	Buildings	Average Daily Flow	Peak Flow
1	Building 'A1' & Building 'A2'	11.80 L/s	37.43 L/s
2	Building 'B'	11.34 L/s	38.60 L/s
3	Building 'Cl' & Building 'C2'	10.20 L/s	33.82 L/s
4	Building 'D'	14.23 L/s	47.06 L/s

#### Table 2 - Sanitary Flow Generation Summary

### 3.4 PROPOSED SANITARY SERVICING

As part of the Walnut Lane extension project, there will be a sanitary sewer installed within the Walnut Lane R.O.W that will be sized to convey flows from the proposed development. The future Walnut Lane sewer will discharge to the 1050 mm diameter trunk sanitary sewer south of the site.

As the subject site is developed, connections from the proposed development to the future sanitary sewer in Walnut Lane will be made via sanitary sewers installed within the site. The following subsections outline the proposed sanitary servicing strategy in detail. Sanitary design sheets and drainage plans corresponding to the proposed sanitary servicing strategy are given in **Appendix A**.

#### 3.4.1 PHASE1

In Phase 1, one sanitary sewer connection that services Buildings 'A1' and 'A2'will be made to the future sanitary sewer on Walnut Lane. Preliminary sizing of the sanitary connection suggests that the connection should be 250 mm diameter. However, the final size will be coordinated with the Mechanical Engineer at the detailed design stage.

According to the topographic surveys prepared by J.D. Barnes Ltd, the existing commercial development in the northwest corner of the site has a sanitary connection to the 200 mm diameter municipal sanitary sewer that runs within an easement on the west boundary of the site. It is proposed that the existing connection to this municipal sanitary sewer be removed during Phase 1 construction. Since the municipal sanitary sewer collects sanitary drainage from the existing commercial development to the west of the site, this municipal sewer must be protected and maintained during all phases of the proposed redevelopment. The survey also shows a sanitary connection directly to Kingston Road for the existing commercial development at the northeast corner of the site. It is proposed that during Phase 1 construction this existing sanitary connection is abandoned.

Refer to **Figure 3B - "Phase 1 Sanitary Servicing"** for an illustration of the proposed sanitary servicing strategy for Phase 1.

#### 3.4.2 PHASE 2

In Phase 2, a public sanitary sewer that connects to the future sanitary sewer on Walnut Lane will be constructed within the proposed public R.O.W west of Building 'B'. This leg of public sanitary sewer will be sized to convey all sanitary flows from Phase 2, Phase 3, and Phase 4. Preliminary sizing suggests that this sewer in the R.O.W should be 375 mm diameter. However, the size will be confirmed during detailed design.

Building 'B' will have one sanitary service connection to the sanitary sewer within the proposed public R.O.W. Preliminary sizing of the sanitary connection suggests that the size should be 200 mm diameter. However, the final size will be coordinated with the Mechanical Engineer at the detailed design stage.

According to the topographic surveys prepared by J.D. Barnes Ltd, the existing commercial development has a sanitary connection to the existing trunk sanitary sewer that runs along the south side of the site. It is proposed that this existing sanitary service connection to the trunk is removed during Phase 2 construction. However, the trunk sanitary sewer must be protected and maintained during all phases of construction.

Refer to **Figure 3C - "Phase 2 Sanitary Servicing"** for an illustration of the proposed sanitary servicing strategy for Phase 2.

#### 3.4.3 PHASE 3

In Phase 3, an extension to the public sanitary sewer proposed in Phase 2 will be made along the proposed public R.O.W south of Buildings 'Cl' and 'C2'. This leg of public sanitary sewer will be sized to convey the sanitary flows from Phases 3 and 4. Preliminary sizing suggests that this sewer should be 375 mm diameter. However, the size will be confirmed during detailed design.

The proposed sanitary sewer in the public R.O.W south of Buildings 'C1' and 'C2' will not be extended along the full length of the R.O.W to the property line on the west side of the development. WSP believes that even with minimal pipe sloping, there is too much length and not enough cover to have a sanitary sewer drain by gravity from the lands to the west and connect to the future sanitary sewer in Walnut Lane. Thus, any future redevelopment within the lands to the west shall direct sanitary flows west to Dixie Road before draining south to the 1050 mm diameter trunk sewer.

One sanitary service connection that services Buildings 'C1' and 'C2' will be made to the sanitary sewer within the proposed R.O.W before the flows are conveyed towards Walnut Lane. Preliminary sizing of the sanitary connection suggests that the connection should be 200 mm diameter. However, the final size will be coordinated with the mechanical engineer at the detailed design stage.

Although no existing buildings will be removed during Phase 3, the topographic surveys prepared by J.D. Barnes Ltd shows that there is an existing 200 mm diameter sanitary connection to the municipal sanitary sewer on the west side of the site that falls within the proposed Phase 3 Lands. It is proposed that this connection be removed as part of the Phase 3 redevelopment, while the existing municipal sewer is to remain.

Refer to **Figure 3D** - **"Phase 3 Sanitary Servicing"** for an illustration of the proposed sanitary servicing strategy for Phase 3.

#### 3.4.4 PHASE 4

In Phase 4, Building 'D' is proposed to have one sanitary service connection to the sanitary sewer within the proposed R.O.W north of the building. Preliminary sizing of the sanitary connection suggests that the connection should be 250 mm diameter. However, the final size will be coordinated with the mechanical engineer at the detailed design stage.

According to the topographic surveys prepared by J.D. Barnes Ltd, the existing commercial development on the south side of the site has a sanitary connection to the 200 mm diameter municipal sanitary sewer that runs along the west boundary of the site. It is proposed that this existing service connection is removed during the Phase 4 redevelopment, while the exiting municipal sanitary sewers are to remain.

Refer to **Figure 3E - "Phase 3 Sanitary Servicing"** for an illustration of the proposed sanitary servicing strategy for Phase 4.

### 3.5 SANITARY CAPACITY ANALYSIS

WSP contacted the Region of Durham regarding the 1050 mm diameter trunk sanitary sewer capacity for a nearby site in October of 2021. At that time, it was indicated that capacity was to be allocated on a first come first serve basis at the time of signing a development agreement. There are currently other ongoing developments within the service area and as such the Region of Durham is in the process of confirming capacity limitations through the use of ongoing flow monitoring. This will form the basis of determining any potential upgrades that will be required as development continues to proceed within the existing sanitary drainage boundary of Pickering City Centre area and beyond.











# **4 STORM DRAINAGE SYSTEM**

A Stormwater Management Report for this development also prepared by WSP has been prepared under a separate cover. It identifies the stormwater controls under which this site will operate to comply all relevant Wet Weather Flow Management Guidelines (WWFMG).

# 4.1 EXISTING CONDITIONS

Based on the record drawings from the Region of Durham, and the topographic surveys prepared by J.D. Barnes Ltd the existing infrastructure in the vicinity of the site is as follows:

- 200 mm 900 mm diameter storm sewers across the site;
- Two quantity control chambers (one within the proposed Phase 1 lands, and one within the proposed Phase 2 lands);
- On site surface storage;
- On site roof storage;
- > One headwall at the south side of the site. This headwall contains two (2) inlets; and
- > 1.83 m x 1.83 m box culvert located at the south end of the site.

In the existing condition, all of the on - site storm sewers ultimately discharge to the 1.83 m x 1.83 m box culvert located at the south end of the site. It is WSP's understanding that the box culvert runs beneath Highway 401 and discharges to a 900 mm culvert under the Go Transit and CNR tracks. It is understood that all flows from the site are ultimately discharged to Frenchman's Bay. Based on the topographic surveys prepared by J.D. Barnes Ltd, it is believed that the existing on - site storm sewers are very shallow due to the outlet elevation and size of the site. The methods of connection are as follows:

- The section of the site that falls within the future Phase 1, and Phase 3 lands drain via the storm network that runs along the west side of the site (herein referred to Existing Storm Network A). Sewers in the main network range from 450 mm diameter to 675 mm diameter in size, and this network has a direct connection to the headwall before discharging to the box culvert. The network also has an existing 150 mm diameter orifice at EX. STM MH 10 that provides quantity control and allows the network to backflow into an on - site quantity control chamber located in the future Phase 3 Lands;
- The section of the site that falls within the future Phase 2, and Phase 4 lands drains through a network that runs along the east and south sides of the site (herein referred to Existing Storm Network B). Sewers in the main network range from 450 mm diameter to 525 mm diameter in size. Based on the topographic surveys prepared by J.D. Barnes Ltd, it is believed that this network discharges directly to the box culvert and avoids the headwall. The network also has an existing 150 mm diameter orifice at EX. STM MH 18 that provides quantity control and allows the network

to backflow into an on - site underground storage chamber located in the future Phase 2 Lands; and

The segment of driveway within the Phase 4 lands that is located west of the headwall drains via a storm network that runs beneath the driveway (herein referred to Existing Storm Network C). The sewers of the main network that fall within the proposed development range from 525 mm diameter to 900 mm diameter and the system has a direct connection to the headwall. Based on the topographic surveys prepared by J.D. Barnes Ltd, it is believed that this storm network west of the headwall collects drainage from Dixie Road and the existing commercial developments to the west.

The existing on - site storm features are illustrated in figure Figure 4A - "Existing Storm Sewers".

## 4.2 PROPOSED MINOR STORM DRAINAGE SYSTEM

As part of the Walnut Lane extension project, there will be a storm network installed within the Walnut Lane R.O.W that will be sized to capture and convey the proposed storm flows within Walnut Lane. The future Walnut Lane sewer will discharge flows to a proposed headwall east of the site. The proposed development will not use the future Walnut Lane storm sewer network to convey its storm flows. Instead, the proposed development will use on - site sewer networks to convey flows to the box culvert located south of the site. The proposed on-site minor storm drainage system will capture all flows up to the 100-year event and release them to the box culvert at the allowable release rate.

The following sections outline the proposed phased storm servicing strategy in detail. Additional details regarding the allowable release rate and overall storm servicing strategy for the site is outlined in the Stormwater Management Report prepared by WSP under a separate cover.

#### 4.2.1 PHASE1

Storm flows from Phase 1 (excluding the park) will be collected by an internal storm drainage system and directed to a storage tank within Building 'A2'. Details regarding the internal drainage system will be determined at the detailed design stage, but the system is to be fit with an OGS to provide the required quality control for the road segments within Phase 1. The storage tank will discharge the flows to a maximum allowable release rate of 161.0 L/s, and it will be designed to hold a volume of 600 m<sup>3</sup>. Preliminary sizing of the storm service connection from the building suggests that the size should be 375 mm diameter. However, the final size will be confirmed at the detailed design stage. Flows from Phase 1 will be directed into Existing Storm Network A.

Storm flows from the Phase 1 park will be captured and controlled by a superpipe fit with a flow control device that will release flows to a maximum allowable release rate of 10.3 L/s. The park flows will be discharged into Existing Storm Network A. Preliminary sizing suggests that this superpipe should be 450 mm in size. However, this will be confirmed at the detailed design stage.

During Phase 1, it is proposed that the existing 10 m - 150 mm diameter orifice that is located on the south side of EX. STM MH 10 be relocated to the east side of the manhole. Relocating the orifice will

provide the same level of quantity control for the existing parking lot east of the manhole that will remain in Phase 1. Since quantity control measures are being proposed in the Phase 1 lands, this orifice will not have to provide quantity control for the future Phase 1 flows.

Preliminary sizing suggests that there will be no upgrades required to Existing Storm Network A to convey the proposed flows from the development in each of the interim conditions described in the subsequent sections. However, in the preliminary analysis it was assumed that there are no flows entering Existing Storm Network A from the commercial lands to the west. It should be noted that the survey shows an existing 300 mm diameter storm sewer connecting to EX. STM MH 9 from the lands to the west. The belief is that this segment of pipe was decommissioned when the lands to the west were redeveloped. If Existing Storm Network A is taking external flows from the west development, then it is likely that storm sewer upgrades will be required. The Phase 1 storm sewer drainage plans and design sheets are included in **Appendix B**.

An infiltration pit located within the Phase 1 Lands is proposed to maintain the pre-development water balance following Phase 1 construction. Preliminary sizing suggests that the pit should have a footprint of 250 m<sup>2</sup>, and a stone depth of 0.85 m. However, the final sizing will be confirmed at the detailed design stage.

Additional details relating to the proposed Phase 1 storm servicing strategy and modelling are included in the Stormwater Management Report prepared by WSP under a separate cover. The proposed storm servicing layout is shown on **Figure 4B - "Phase 1 - Storm Servicing".** 

#### 4.2.2 PHASE 2

Storm flows from Phase 2 (excluding the R.O.W) will be collected by an internal storm drainage system and directed to a storage tank within Building 'B'. Specifications regarding the internal drainage system will be determined at the detailed design stage, but the system is to be fit with an OGS to provide the required quality control for the private road segments within Phase 2. The storage tank will discharge the flows to a maximum allowable release rate of 120.7 L / s and will have a storage volume of 500 m<sup>3</sup>. A storm connection will be made from Building 'B' to Existing Storm Network B. Preliminary sizing of the storm connections suggests that the connection should be 375 mm diameter. However, the final size will be confirmed at the detailed design stage.

To avoid backflow into proposed Building 'B', the 10m-250 mm diameter orifice on the northeast side of STM MH 18 will be removed. Remodelling the system without the orifice and backflow suggests that the existing 525 mm diameter sewers will need to be upgraded to sizes ranging from 675 to 750 mm diameter. In the analysis it was assumed that the existing pipe slopes measured from the topographic surveys prepared by J.D. Barnes Ltd would be maintained. The Phase 2 storm sewer drainage plans and design sheets that were developed in the analysis are included in **Appendix B**.

Storm flows from the Phase 2 R.O.W will be conveyed west across the site by a superpipe into Existing Storm Network A. The superpipe will be fit with a flow control device to discharge at a maximum allowable release rate of 15.3 L / s. Preliminary sizing suggests that this superpipe should be 1050 mm diameter to handle the future flows. However, the sizing will be confirmed at the detailed design stage.

An infiltration pit located within the Phase 2 lands is proposed to maintain the pre-development water balance following Phase 2 construction. Preliminary sizing suggests that the pit should have a footprint of 324 m<sup>2</sup>, and a stone depth of 0.49 m. However, the final sizing will be confirmed at the detailed design stage.

Additional details relating to the proposed Phase 2 storm strategy and modelling are included in the Stormwater Management Report prepared by WSP under a separate cover. The proposed storm servicing layout is shown on **Figure 4C - "Phase 2 - Storm Servicing"**.

#### 4.2.3 PHASE 3

Storm flows from Phase 3 (excluding the R.O.W) will be collected by an internal storm drainage system and directed to a storage tank within Building 'C2'. Specifications regarding the internal drainage system will be determined at the detailed design stage, but the system is to be fit with an OGS to provide the required quality control for the private road segments within Phase 3. The storage tank will discharge the flows to a maximum allowable release rate of 138.80 L / s and will have a volume of 700.0 m<sup>3</sup>. A storm connection will be made from Building 'C2' to the proposed 1050 mm diameter superpipe within the proposed R.O.W before discharging to Existing Storm Network A. Preliminary sizing of the storm service connection suggests that it should be 375 mm diameter. However, the final size will be confirmed at the detailed design stage.

Storm flows from the Phase 3 park will be captured and controlled by a superpipe fit with a flow control device that will release flows to a maximum allowable release rate of 6.6 L / s. Preliminary sizing suggests that this superpipe should be 450 mm in diameter. However, this will be confirmed at the detailed design stage. Flows from the park will also be conveyed into the superpipe within the proposed R.O.W before entering Existing Storm Network A.

Storm flows from the Phase 3 R.O.W will be conveyed into the proposed superpipe located within the R.O.W. With the contribution of the controlled flows of Phase 3, the maximum allowable release rate of the superpipe will increase to 200.4 L/s. The Phase 3 storm sewer drainage plans and design sheets that were developed in the analysis are included in **Appendix B**.

An infiltration pit located within the Phase 3 Lands is proposed to maintain the pre-development water balance following Phase 3 construction. Preliminary sizing suggests that the pit should have a footprint of 380 m<sup>2</sup>, and a stone depth of 0.61 m. However, the final sizing will be confirmed at the detailed design stage.

Additional details relating to the proposed Phase 3 storm servicing strategy and modelling are included in the Stormwater Management Report prepared by WSP under a separate cover. The proposed storm servicing layout is shown on **Figure 4C - "Phase 3 - Storm Servicing".** 

#### 4.2.4 PHASE 4

Storm flows within Phase 4 that are from north of the proposed driveway, and east of the proposed park will be collected by an internal storm drainage system and directed to a storage tank within Building 'D'. Specifications regarding the internal drainage system will be determined at the detailed

design stage, but the system is to be fit with an OGS to provide the required quality control for the any road segments within the phase that are north of the proposed building. The storage tank will discharge the flows to a maximum allowable release rate of 131.7 L / s and will have a storage volume of 600 m<sup>3</sup>. A storm service connection will be made from Building 'D' to Existing Storm Network B. Preliminary sizing of the storm connections suggest that it should be 375 mm diameter. However, the final size will be confirmed at the detailed design stage.

Storm flows within Phase 4 that are tributary to the private road east of the headwall, are proposed to flow into Existing Storm Network B using the existing catch basins within the driveway. The intention with this strategy is to match the existing condition, and re-use as many of the existing catch basins and as possible. Quality control for this area will be provided by the existing OGS located at EX. STM MH 17.

Storm flows within the Phase 4 park will be captured and controlled by a superpipe fit with a flow control device that will release flows to a maximum allowable release rate of 22.6 L / s. Preliminary sizing suggests that this superpipe should be 600 mm in diameter. However, this will be confirmed at the detailed design stage. The park will then have a storm connection that also conveys flow directly to Existing Storm Network B.

For the section of Phase 4 private road that is located west of the headwall, the intention is to match the existing condition and have this area drain to the headwall via Existing Storm Network C.

An infiltration pit located within the Phase 4 Lands is proposed to maintain the pre-development water balance following Phase 4 construction. Preliminary sizing suggests that the pit should have a footprint of 484 m<sup>2</sup>, and a stone depth of 0.44 m. However, the final sizing will be confirmed at the detailed design stage.

The Phase 4 design sheets and sewer analysis are included in **Appendix B**. Since the intention is to match the existing condition west of the headwall and preserve all of Existing Storm Network C, this segment of the network was excluded from the analysis.

### 4.3 MAJOR STORM DRAINAGE SYSTEM

The major storm system is a conveyance system for flows in excess of the minor system flows. Stormwater run-off from events up to and including the 100 - year storm event will be contained on site and released at a controlled rate within the allowable post-development limits to the minor storm system. For major storm events exceeding the 100 - year storm, overland flow routes will be designed to direct excess flows to the existing culvert at the south end of the site via the on - site roadways.

For the development of the site, the grading design will be prepared such that the surface (i.e., roads, walkways and landscaped areas) grades will direct surface drainage away from the building to approved outlets. The proposed grading of the subject site will ensure that existing grade elevations at the time of construction will be met along the property limits. The plumbing system for each building will be coordinated with the mechanical consultant to ensure that they are designed to convey a 100-year run-off from the development. For major storm events exceeding the 100 - year storm and the capacity of the proposed storage tanks, an overflow will be designed to direct excess flows to grade

and ultimately to the existing box culvert at the south end of the site via the on - site roadways. Refer to **Appendix C** for the preliminary site grading plan.










Figure 4-A – Existing Storm Sewers

# **5 SITE GRADING**

## 5.1 EXISTING CONDITIONS

In the existing condition the site falls from north to south. Runoff is conveyed away from the existing buildings to a series of on – site drains. In the emergency situation where runoff cannot be captured, it is conveyed to the existing box culvert located at the south end of the site via the on - site driveways.

## 5.2 PROPOSED CONDITIONS

The proposed grading design for the new development will direct storm drainage to the on - site collection points. Since the site grading will be phased, the objective is to capture as much runoff within each phase as possible and prevent overland flow to the existing property. However, since the existing site falls from north to south, the emergency overland flow route for the major storm events must go through the existing site towards the box culvert located at the south end of the site. This flow will be via the on - site driveways and R.O.W's and it will ensure that drainage is diverted away from all of the buildings.

The proposed grading plans for each phase are included in **Appendix C**. In summary the plans consider the following:

- Proposed grades along all boundaries (phase and site) are to match to existing so that there is no impact to the adjacent properties;
- Minimize disruption to all existing municipal rights-of-way containing existing utilities and services;
- Promote drainage into the minor sewer systems;
- Grade the lands to direct overland flow away from the proposed structures;
- Create high points within the development area to direct flows towards drainage inlets with a maximum proposed ponding depth of 0.30 m; and
- Ensure that minimum and maximum grades conform to AODA and City of Pickering standards.

# **6 EROSION AND SEDIMENT CONTROL**

Temporary Erosion and Sediment Control must be provided onsite during construction to prevent sediment runoff to the neighbouring developments and municipal roads. Fencing and hoarding will be erected surrounding the perimeter of each phase, and mud mats will be required at site access points. In addition, catchbasins that are to remain in close proximity to the construction zones will be protected with geotextile fabric. All Erosion and Sediment Control Best Management Practices shall be designed, constructed and maintained for the duration of construction. The proposed Erosion and Sediment Control Plans for each phase are outlined in **Appendix D**.

# 7 CONCLUSIONS

## 7.1 WATER

The proposed development will rely on the future 300mm diameter watermain in Walnut Lane for water servicing. At this time. it is WSP's understanding that this watermain will have the capacity to service the proposed development. Buildings within the proposed development will either have service connections directly to the watermain in Walnut Lane, or to the proposed extension of the watermain along the future 20.0m R.O.W that is proposed within the site. Each building's water service connection will at minimum consist of one domestic connection and one fire connection. If the height of any building exceeds 84 m, a secondary fire connection will be provided as per Ontario's building code requirements. The service connection sizing will be coordinated with the Region of Durham and the mechanical engineering consultant at the detailed design stage. The connections will be made in accordance with Region of Durham standards.

## 7.2 SANITARY

Sanitary flows from the proposed development will be conveyed to the future sanitary sewer that will be installed in Walnut Lane. The Walnut Lane sanitary sewer has been sized to convey flows from the proposed development to the existing 1050 mm diameter trunk sanitary sewer that runs along the south side of the site. For a nearby development, WSP was informed by the Region of Durham that the capacity for the trunk sewer was to be allocated on a first come first serve basis at the time of signing a development agreement. It is WSP's understanding that there are currently other ongoing developments within the service area and as such the Region of Durham is in the process of confirming capacity limitations through use of ongoing flow monitoring. This will form the basis of determining any potential upgrades that will be required as development continues to proceed within the existing sanitary drainage boundary of Pickering City Centre area and beyond. Thus, it is assumed that at the time of the proposed redevelopment of the subject lands, there will be capacity in the trunk sewer to accept the proposed sanitary flows.

## 7.3 STORM

All storm flows from the site up to the 100-year event will ultimately be released at the allowable release rate to the 1.83 m x 1.83 m box culvert located at the south end of the site. On site quantity control chambers and superpipes will be used to provide the necessary quantity controls throughout the site.

Storm flows from Phases 1 and 3, and the proposed 20.0m R.O.W will be conveyed into Existing Storm Network A on the west side of the site. Preliminary sizing suggests that Existing Storm Network A has enough capacity to convey the flows to the box culvert in each of the proposed conditions.

Storm flows from Phase 2 (excluding the R.O.W) and flows within Phase 4 that are east of the headwall will be conveyed into Existing Storm Network B that runs along the south side of the site. Preliminary sizing suggests that minor pipe upgrades to Existing Storm Network B will be required to accommodate the proposed flows.

Storm flows within Phase 4 that are tributary to west of the headwall will flow to the box culvert via Existing Storm Network C (southwest side of the site) matching the existing condition.

Water balance will be addressed on a phase-by-phase basis using infiltration pits that will be installed within the limits of each phase.



# AND DESIGN SHEETS

#### PHASE 1

1101A, 1105, and 1163 KINGSTON ROAD 221-12931 Project: Job No.:

Building	Unit Count/ GFA (ha)	Site Area (ha)	Occupancy Rate	Equivalent Population	Per Capita Flow	Average Daily Flow (L/s)	Peaking Factor	Peak Flow (L/s)
			Building	A1				
Residential	609			1214	364 L/cap/day	5.11	3.74	19.15
1B	359		1.5 ppu	539				
2B	201		2.5 рри	503				
3B	49		3.5 рри	172				
Retail	0.49				180000 L/ha/day	1.03	1.00	1.03
Infiltration		1.02				0.27		0.27
Subtotal				1214		6.41		20.45
			Building	A2				
Residential	602			1199	364 L/cap/day	5.05	3.75	18.93
1B	355		1.5 рри	533				
2B	199		2.5 ppu	498				
3B	48		3.5 рри	168				
Daycare	0.07				180000 L/ha/day	0.15	1.00	0.15
Infiltration		0.74				0.19		0.19
Subtotal				1199		5.39		19.27
Phase 1 Residential Subtotal				2413	364 L/cap/day	10.17	3.52	35.79
Phase 1 Retail/Daycare Subtotal	0.57				180000 L/ha/day	1.18	1.00	1.18
Phase 1 Infiltration		1.76				0.46		0.46
PHASE 1 TOTAL						11.80		37.43

Notes: 1. Occupancy rates, per capita flows and peaking factor are as per the Region of Durham Design Specifications For Sanitary Sewers 2. Unit Counts and Floor Areas from drawings prepared by Turner Fleisher, dated October 23, 2023 3. Infiltration considered for entire Phase area to account for any future changes in plan

### PHASE 2

Project: Job No.:

## 1101A, 1105, and 1163 KINGSTON ROAD 221-12931

Building	Unit Count/ GFA (ha)	Site Area (ha)	Occupancy Rate	Equivalent Population	Per Capita Flow	Average Daily Flow (L/s)	Peaking Factor	Peak Flow (L/s)
			Building	В				
Residential	1303			2593	364 L/cap/day	10.92	3.50	38.18
1B	769		1.5 ppu	1154				
2B	430		2.5 ppu	1075				
3B	104		3.5 ppu	364				
Retail	0.00				180000 L/ha/day	0.00	1.00	0.00
Infiltration		1.61				0.42		0.42
Subtotal				2593		11.34		38.60
Phase 2 Residential Subtotal				2593	364 L/cap/day	10.92	3.50	38.18
Phase 2 Retail Subtotal	0.00				180000 L/ha/day	0.00	1.00	0.00
Phase 2 Infiltration		1.61				0.42		0.42
PHASE 2 TOTAL						11.34		38.60

Notes:

Cocupancy rates, per capita flows and peaking factor are as per the Region of Durham Design Specifications For Sanitary Sewers
 Unit Counts and Floor Areas from drawings prepared by Turner Fleisher, dated October 23, 2023
 Infiltration considered for entire Phase area to account for any future changes in plan

#### PHASE 3

Project: Job No.:

#### 1101A, 1105, and 1163 KINGSTON ROAD 221-12931

Building	Unit Count/ GFA (ha)	Site Area (ha)	Occupancy Rate	Equivalent Population	Per Capita Flow	Average Daily Flow (L/s)	Peaking Factor	Peak Flow (L/s)
			Building C1	& C2				
Residential	1103			2195	364 L/cap/day	9.25	3.55	32.87
1B	651		1.5 ppu	977				
2B	364		2.5 ppu	910				
3B	88		3.5 ppu	308				
Retail	0.22				180000 L/ha/day	0.46	1.00	0.46
Infiltration		1.91				0.50		0.50
Subtotal				2195		10.20		33.82
Phase 3 Residential Subtotal				2195	364 L/cap/day	9 25	3 55	32 87
Phase 3 Retail Subtotal	0.22			_100	180000 L/ha/day	0.46	1.00	0.46
Phase 3 Infiltration		1.91				0.50		0.50
PHASE 3 TOTAL						10.20		33.82

Notes:

Occupancy rates, per capita flows and peaking factor are as per the Region of Durham Design Specifications For Sanitary Sewers
 Unit Counts and Floor Areas from drawings prepared by Turner Fleisher, dated October 23, 2023
 Infiltration considered for entire Phase area to account for any future changes in plan
 Individual unit breakdowns for Buildings C1 and C2 were not available at the time of writing this report

#### PHASE 4

Project: Job No.:

## 1101A, 1105, and 1163 KINGSTON ROAD 221-12931

Building	Unit Count/ GFA (ha)	Site Area (ha)	Occupancy Rate	Equivalent Population	Per Capita Flow	Average Daily Flow (L/s)	Peaking Factor	Peak Flow (L/s)
			Building	D				
Residential	1621			3226	364 L/cap/day	13.59	3.42	46.42
1B	957		1.5 ppu	1436				
2B	535		2.5 ppu	1338				
3B	129		3.5 ppu	452				
Retail	0.00				180000 L/ha/day	0.00	1.00	0.00
Infiltration		2.47				0.64		0.64
Subtotal				3226		14.23		47.06
Phase 4 Residential Subtotal				3226	364 L/cap/day	13.59	3.42	46.42
Phase 4 Retail Subtotal	0.00				180000 L/ha/day	0.00	1.00	0.00
Phase 4 Infiltration		2.47				0.64		0.64
PHASE 4 TOTAL						14.23		47.06

Notes:

Cocupancy rates, per capita flows and peaking factor are as per the Region of Durham Design Specifications For Sanitary Sewers
 Unit Counts and Floor Areas from drawings prepared by Turner Fleisher, dated October 23, 2023
 Infiltration considered for entire Phase area to account for any future changes in plan



WSP CANADA INC.

## THE REGIONAL MUNICIPALITY OF DURHAM SANITARY SEWER DESIGN SHEET

PROJ JOB I FROM	JECT : No. : M :		<u>1101A, 110</u> 221-12931-	05, and 1163 K -00	INGSTON F	ROAD_		Phase 1						DESIGNE CHECKEI DATE :	D BY: D BY :	<u>ZB</u> <u>KK</u> 2023-10-25					
			Residential			С	ommerc	cial	Industrial	Institutional			Flow in L/	's				Proposed	Sewer		
MH.		Gross	Population	Population	Peak	Lot	Floor	Floor	Lot	Lot	Res.	flow	Comm.	Indus.	Inst.	Total	Actual	Slope	Capacity	Velocity	
No.		area	density		flow	area	space	area	area	(ha)	Infil*	Sewage				flow	Pipe	%	in	in	Load
		(ha)			factor	(ha)	Index	(ha)			L/S 0.26	L/S 0.0042	L/S 2.08	L/S 1.04	L/S 1.30	L/s	size mm		L/s	m/s	%
BLDG	A1 & A2	1.76		2413				0.57													
SAN	MH1A	1.76		2413	3.52			0.57			0.46	35.79	1.18	0.00	0.00	37.43	250	2.00	84.10	1.71	45%
SAN N	/H1A	0.00		0				0.00													
SAN	MH2A	1.76		2413	3.52			0.57			0.46	35.79	1.18	0.00	0.00	37.43	200	2.00	46.38	1.48	81%
SAN N	ЛН2А	0.00		0				0.00													
FUT.	SAN MH-SA1	1.76		2413	3.52			0.57			0.46	35.79	1.18	0.00	0.00	37.43	375	0.50	123.98	1.12	30%

Notes:

Occupancy rates, per capita flows and peaking factor are as per the Region of Durham Design Specifications For Sanitary Sewers
 Unit Counts and Floor Areas from drawings prepared by Turner Fleisher, dated October 23, 2023

3. Infiltration considered for entire Site Area to account for any future changes in plan

<u>ZB</u>
<u>KK</u>
2023-10-25

WSP CANADA INC.

## THE REGIONAL MUNICIPALITY OF DURHAM SANITARY SEWER DESIGN SHEET

	PROJECT : JOB No. : FROM :		<u>1101A, 110</u> 221-12931-	05, and 1163 K -00	INGSTON R	OAD_	F	Phase 2-4						DESIGNE CHECKE DATE :	ED BY: D BY :	<u>ZB</u> <u>KK</u> 2023-10-25					
			Residential			C	ommercia	al	Industrial	Institutional			Flow in L	/s				Proposed	Sewer		
	MH. No.	Gross area (ha)	Population density	Population	Peak flow factor	Lot area (ha)	Floor space Index	Floor area (ha)	Lot area	Lot (ha)	Res. Infil* L/S 0.26	flow Sewage L/S 0.0042	Comm. L/S 2.08	Indus. L/S 1.04	Inst. L/S 1.30	Total flow L/s	Actual Pipe size mm	Slope %	Capacity in L/s	Velocity in m/s	Load %
BL	DG D	2.47		3226			C	0.00													
	SAN MH 3A	2.47		3226	3.42			0.00			0.64	46.42	0.00	0.00	0.00	47.06	250	2.00	84.10	1.71	56%
SA	N MH 3A	0.00		0			C	).00													
	SAN MH 5A	2.47		3226	3.42			0.00			0.64	46.42	0.00	0.00	0.00	47.06	250	2.00	84.10	1.71	56%
BL	L DG C1 & C2	1.91		2195			C	).22													
	SAN MH 4A	1.91		2195	3.55			0.22			0.50	32.87	0.46	0.00	0.00	33.82	200	2.00	46.38	1.48	73%
<u>S</u> A	N MH 4A	0.00		0			C	0.00													
	SAN MH 5A	1.91		2195	3.55			0.22			0.50	32.87	0.46	0.00	0.00	33.82	200	2.00	46.38	1.48	73%
SA		0.00		0			C	).00													
	SAN MH 6A	4.38		5421	3.21			0.22			1.14	73.36	0.46	0.00	0.00	74.96	375	0.50	123.98	1.12	60%
BL	L DG B	1.61		2593			c	0.00													
	SAN MH 6A	1.61		2593	3.50			0.00			0.42	38.18	0.00	0.00	0.00	38.60	200	2.00	46.38	1.48	83%
SA		0.00		0			C	0.00													
	SAN MH 7A	5.99		8014	3.05			0.22			1.56	102.96	0.46	0.00	0.00	104.97	375	0.50	123.98	1.12	85%
SA		0.00		0			C	0.00													
	SAN MH 8A	5.99		8014.00	3.05			0.22			1.56	102.96	0.46	0.00	0.00	104.97	375	0.50	123.98	1.12	85%
SA	 N MH 8A	0.00		0			c	0.00													
	FUT. SAN MH-SA12	5.99		8014.00	3.05			0.22			1.56	102.96	0.46	0.00	0.00	104.97	375	0.50	123.98	1.12	85%

Notes:

Occupancy rates, per capita flows and peaking factor are as per the Region of Durham Design Specifications For Sanitary Sewers
 Unit Counts and Floor Areas from drawings prepared by Turner Fleisher, dated October 23, 2023

3. Infiltration considered for entire Site Area to account for any future changes in plan WSP CANADA INC.



# B STORM FLOW CALCULATIONS AND DESIGN SHEETS













EXISTING CATCHMENTS DELINEATED USING TOPO BY J.D BARNES LIMITED DATED FEBRUARY 2, 2023 AND STORMWATER MANAGEMENT REPORT BY a.m candaras associates inc. DATED JANUARY 2015





																					PREPARED BY:	Z.B.
										STORM SEW	ER DESIGN SHEE	ET									CHECKED BY:	К.К.
WSP CANADA INC.									11	01A, 1105, and 1163	KINGSTON ROAD	D - PHASE 1									DATE:	25-Oct-23
																					LAST PRINTED:	25-Oct-23
										City	of Pickering										FILE No	221-12931
			CATCHMENT	ha	R	2.78	ACCUM	Tc	i	Q <sub>100</sub>	Q <sub>CON</sub>	Q <sub>TOTAL</sub>	PIPE					TIME IN	TOTAL			
STREET	FROM	то	ID.	AREA	RUNOFF COEFFICIEN	A.R.	2.78		RAINFAI	LL PEAK UNCONTROLLED FLC	OW CONTROLLED FLOW	Q <sub>100</sub> + Q <sub>CON</sub>	DIA.	SLOPE	LENGTH	CAPACITY	VELOCITY	SECTION	TIME	LOAD		COMMENTS
	M.H.	M.H.					A.R.	( MIN )	INTENSI	TY (L/S)	(L/S)	(L/S)	( mm )	(%)	(m)	(L/s)	(m/s)	( min. )	( min. )	%		
				Mixed/Use	e				( mm / h	r) <b>EA</b>												
				1					1				1			1			1			
Phase 1	PHASE 1 SWM TANK	STM MH 1	PH 1	1.66	0.95	4.38	4.38	10.00	186.6	9 -	161.00	161.00	375	2.00	16.7	247.95	2.25	0.12	10.12	65%	- PH1 ALLOWABI	E REALEASE RATE
Phase 1	PHASE 1 PARK SUPERPIP	E STM MH 1	PARK 1	0.10	0.25	0.07	0.07	10.00	186.6	9 -	10.30	10.30	450	-	_	-	-	-	-	-	- SUPERPIPE WIT	H FLOW CONTROL
										-											- ALLOWABLE RE	LEASE RATE
Phase 1	STM MH 1	EX STM MH 10	) -	-	-	-	4.45	10.12	185.4	9 -	171.30	171.30	450	0.50	10.3	201.60	1.27	0.14	10.26	85%	- PH1 + PH1 PARI 201 & 202 IN SWN	ALLOWABLE RELEASE RATE REFER TO CATCHMENTS FIGURE 3
Existing Development	EX STM MH 29	EX STM MH 10	EX. 1	1.69	1.00	4.70	4.70	10.00	186.6	9 -	88.25	88.25	150	0.87	10.0	14.22	0.80	0.21	10.21	-	Q=CA (2gh)^0.5 WHERE: C = 0.8 ( m/s^2, h= 85.10 (H STORMWATER M (PROPOSED NE 1 Q=0.8*0.0177m^2' Q=0.08825m^3/s Q= 88.25 L/s	prifice tube), A = 0.0177m <sup>2</sup> (150 mm DIA. ORIFICE), g = 9.81 IGH WATER LEVEL PER a.m candaras associates inc ANAGEMENT REPORT DATED JANUARY, 2015) - 83.12 VV. AFTER ORIFICE RELOCATION) = 1.98m (2*9.81m/s^2*1.98m)
Existing Development	EX STM MH 10	EX STM MH 9	-	-	-	-	9.15	10.26	184.1	9 -	259.55	259.55	600	0.68	46.8	506.33	1.79	0.44	10.70	51%	- PIPE SLOPE ME SURVEY PREPAR	ASURED FROM INVERT INFORMATION PROVIDED IN SITE ED BY J.D BARNES DATED FEB 2, 2023
Existing Development	EX STM MH 9	EX STM MH 8 (OGS)	-	-	-	-	9.15	10.70	180.1	5 -	259.55	259.55	600	0.60	9.4	475.61	1.68	0.09	10.79	55%	- PIPE SLOPE AS WATER MANAGE BECAUSE SURVE SEGMENT. SLOP	PER a.m candaras associates inc. "SITE SERVICING & STORM MENT PLAN" DATED May 21, 2010. DESIGN INFO USED Y CONTAINS CONFLICTING INFORMATION THROUGH THIS E TO BE VERIFIED DURING DETAILED DESIGN.
Existing Development	EX STM MH 8 (OGS)	EX STM MH 7	-	-	-	-	9.15	10.79	179.3	2 -	259.55	259.55	600	0.60	7.4	475.61	1.68	0.07	10.86	55%	- PIPE SLOPE AS WATER MANAGE BECAUSE SURVE SEGMENT. SLOP	PER a.m candaras associates inc. "SITE SERVICING & STORM MENT PLAN" DATED May 21, 2010. DESIGN INFO USED Y CONTAINS CONFLICTING INFORMATION THROUGH THIS E TO BE VERIFIED DURING DETAILED DESIGN.
Existing Development	EX STM MH7	EX STM MH 6	-	-	-	-	9.15	10.86	178.6	6 -	259.55	259.55	600	0.39	51.1	383.45	1.36	0.63	11.49	68%	- PIPE SLOPE ME SURVEY PREPAR - UPSIZE EX. 600 FUTURE PHASES	ASURED FROM INVERT INFORMATION PROVIDED IN SITE ED BY J.D BARNES DATED FEB 2, 2023 nm DIA. SEWER TO 675mm DIA. TO ACCOMMODATE
Existing Development	EX STM MH 6	Headwall	-	-	-	-	9.15	11.49	173.2	6 -	259.55	259.55	675	0.39	35.6	524.95	1.47	0.40	11.89	49%	- PIPE SLOPE UN SLOPE TO BE VE	KNOWN, ASSUMED SAME SLOPE AS UPSTREAM PIPE. RIFIED DURING DETAILED DESIGN.
*i <sub>100</sub> =2096.425/(T <sub>c</sub> +6.485)^0.863	NOTE: UNCONTROLLED R	UNOFF COEFFIC	CIENTS ARE SC	ALED B	Y FACTOR OF	1.25 (TC	D MAX V	ALUE (	OF 1) A	S PER PICKERING S	TANDARDS											

### RUNOFF COEFFICIENTS

0.25 0.50 SOFT LANDSCAPING/PARK

GREEN ROOF

0.95 IMPERVIOUS AT GRADE 0.95 IMPERVIOUS ROOF

0.90 0.90 No. OF SHEETS

WSP CANADA INC.

STORM SEWER DESIGN SHEET 1101A, 1105, and 1163 KINGSTON ROAD - PHASE 2 City of Pickering CATCHMENT ha R 2.78 ACCUM Q<sub>100</sub> QCON QTOTA PIPE TIME IN TOTAL AREA A.R. SECTION TIME (min.) STREET то ID. RUNOFF COEFFICIE 2.78 RAINFALL PEAK UNCONTROLLED FL CONTROLLED FLOV DIA. SLOPE LENGTH CAPACITY FROM ELOCIT LOAD Q<sub>100</sub> + Q<sub>CON</sub> мн M.H. A.R. (MIN) INTENSITY (L/S) (L/S) (L/S) (mm) (%) (m) (L/s) (m/s) (min) % ( mm / hr ) EAST SITE 375 2.00 16.7 247.95 2.25 0.12 65% PHASE 1 SWM TANK STM MH 1 PH 1 1.66 0.95 4.38 4.38 10.00 186.69 161.00 161.00 10.12 Phase 1 -0.07 0.07 10.00 186.69 PHASE 1 PARK SUPERPIPE STM MH 1 0.10 450 Phase 1 PARK 1 0.25 10.30 10.30 --------EX STM MH 10 4.45 10.12 185.49 171.30 450 0.50 10.3 1.27 0.14 10.26 85% STM MH 1 171.30 201.60 Phase 1 -Q= WF m/s STC (PR Q=0 Q=0. Q= 8 EX STM MH 10 150 0.87 0.80 0.21 EX. MH29 EX. 1 1.69 0.95 4.46 4.46 10.00 186.69 10.0 14.22 10.21 Existing Development -88.25 88.25 -EX STM MH 9 600 0.68 46.8 1.79 0.44 10.70 Existing Development EX STM MH 10 8.92 10.26 184.19 259.55 259.55 506.33 51% ----. Existing Development STM MH 2 STM MH 9 ROW 1 0.27 0.95 0.71 0.71 10.00 186.69 15.30 15.30 1050 0.00 205.7 0.00 0.00 --Existing Development STM MH9 EX STM MH 9 0.71 10.00 186.69 525 0.30 10.1 235.55 1.09 0.15 10.15 6% ---15.30 15.30 EX STM MH 8 Existing Development EX STM MH 9 9.62 10.70 180.15 274.85 274.85 600 0.60 9.4 475.61 1.68 0.09 10.79 58% -(OGS) Existing Development EX STM MH 8 (OGS) EX STM MH 7 9.62 10.79 179.32 274.85 274.85 600 0.60 7.4 475.61 1.68 0.07 10.86 58% W. BE ----EX STM MH7 EX STM MH 6 9.62 10.86 178.66 600 0.39 51.1 1.36 0.63 11.49 72% Existing Development -----274.85 274.85 383.45 Existing Development EX STM MH 6 Headwall 9.62 11.49 173.26 274.85 274.85 675 0.39 35.6 524.95 1.47 0.40 11.89 52% SOUTH SITE 
 375
 2.00
 18.2
 247.95
 2.25
 0.14
 10.14
 49%
 - PH

 375
 1.00
 19.8
 175.33
 1.59
 0.21
 10.34
 69%
 PHASE 2 SWM TANK STM MH 3 Phase 2 PH 2 1.24 0.87 3.00 3.00 10.00 186.69 120.70 120.70 120.70 Phase 2 STM MH 3 EX STM MH 23 3.00 10.14 185.38 120.70 --Existing Development EX STM MH 20 EX STM MH 23 EX. 2 0.28 1.00 0.78 0.78 10.00 186.69 145.32 0.00 145.32 525 0.35 31.2 254.43 1.18 0.44 10.44 57% 1.71 0.20 Existing Development EX BUILDING EX STM MH 23 EX. 4 1.01 1.00 2.81 2.81 10.00 186.69 -43.40 43.40 250 2.00 21.0 84.10 10.20 52% Existing Development EX STM MH 23 EX STM MH 19 EX. 3 0.10 0.80 0.22 1.00 10.44 182.47 182.62 164.10 346.72 675 0.29 88.8 452.67 1.26 1.17 11.61 77% Existing Development EX STM MH 19 EX STM MH 18 EX. 5 0.31 0.90 0.78 1.78 11.61 172.25 305.99 164.10 470.09 750 0.23 83.3 533.91 1.21 1.15 12.76 88% EX STM MH 17 609.77 1.38 0.16 EX STM MH 18 1.78 12.76 163.34 750 0.30 13.3 12.92 74% Existing Development ----290.16 164.10 454.26 - L IF Existing Development EX STM MH 17 BOX CULVERT 1.78 12.92 162.17 288.09 164.10 454.26 750 0.39 695.24 1.57 65% ---PR AN SE

100=2096.425/(T<sub>c</sub>+6.485)^0.863

NOTE: UNCONTROLLED RUNOFF COEFFICIENTS ARE SCALED BY FACTOR OF 1.25 (TO MAX VALUE OF 1) AS PER PICKERING STANDARDS

RUNOFF COEFFICIENTS

0.25	SOFT LANDSCAPING/PARK	0.95	IMPERVIOUS AT GRADE	0.90	No. OF SHEETS
0.50	GREEN ROOF	0.95	IMPERVIOUS ROOF	0.90	1

PREPARED BY:	Z.B.
CHECKED BY:	K.K.
DATE:	25-Oct-23
LAST PRINTED:	25-Oct-23
FILE No	221-12931
	COMMENTS
LLOWABLE RI	ELEASE RATE
H1 + PH1 PAR 202 IN SWM FI	K ALLOWABLE RELEASE RATE REFER TO CATCHMENTS 201 GURE 3
CA (2ab)00 E (	
CA (2017-0.5 ( IERE: C = 0.8 s^2, h= 85.10 (I ORMWATER N ROPOSED NE 0.8*0.0177m^2 0.08825m^3/s 88.25 L/s	Onice Equation), A = 0.0177m*2 (150 mm DIA. ORIFICE), g = 9.81 HIGH WATER LEVEL PER a.m candaras associates inc ANAGEMENT REPORT DATE JANUARY, 2015) - 83.12 INV. AFTER ORIFICE RELOCATION) = 1.98m *(2*9.81m/s*2*1.98m)
IPE SLOPE ME	EASURED FROM INVERT INFORMATION PROVIDED IN SITE
RVEY PREPA	RED BY J.D BARNES DATED FEB 2, 2023
PROPOSED FL D.W. REFER T HASE 2 ROW	AT 1050mm DIA. SUPERPIPE ACROSS SITE WITHIN PHASE 3 O SWM REPORT FOR MODELLING DETAILS ALLOWABLE RELEASE RATE
IPE SLOPE AS ATER MANAGE CAUSE SURVI GMENT. SLOF	PER a.m candaras associates inc. "SITE SERVICING & STORM IMENT PLAN" DATED May 21, 2010. DESIGN INFO USED EY CONTAINS CONFLICTING INFORMATION THROUGH THIS "E TO BE VERIFIED DURING DETAILED DESIGN.
IPE SLOPE AS ATER MANAGE CAUSE SURV GMENT. SLOF	PER a.m candaras associates inc. "SITE SERVICING & STORM MENT PLAN" DATED May 21, 2010. DESIGN INFO USED EY CONTAINS CONFLICTING INFORMATION THROUGH THIS "E TO BE VERIFIED DURING DETAILED DESIGN.
IPE SLOPE ME RVEY PREPAI	EASURED FROM INVERT INFORMATION PROVIDED IN SITE RED BY J.D BARNES DATED FEB 2, 2023
IPE SLOPE UN OPE TO BE VE	IKNOWN, ASSUMED SAME SLOPE AS UPSTREAM PIPE. RIFIED DURING DETAILED DESIGN.
H2 ALLOWABI	LE REALEASE RATE
EFER TO EX. : IPE SLOPE ME RVEY PREPAI	2 IN PHASE 2 STORM DRAINAGE PLAN EASURED FROM INVERT INFORMATION PROVIDED IN SITE RED BY J.D BARNES DATED FEB 2, 2023
EFER TO EX. ONTROLLED I RVICING & ST	4 IN PHASE 2 STORM DRAINAGE PLAN. RELEASE RATE AS PER a.m. candaras associates inc. "SITE ORM WATER MANAGEMENT PLAN" DATED May 21, 2010.
EFER TO EX. 3 PGRADE EX. 3 IPE SLOPE ME RVEY PREPAI	3 IN PHASE 2 STORM DRAINAGE PLAN. 325mm DIA. SEWER TO 675mm DIA. ASURED FROM INVERT INFORMATION PROVIDED IN SITE RED BY J.D BARNES DATED FEB 2, 2023
EFER TO EX. 9 PGRADE EX. 9 IPE SLOPE ME RVEY PREPAI	5 IN PHASE 2 STORM DRAINAGE PLAN. 525mm DIA. SEWER TO 750mm DIA. CASURED FROM INVERT INFORMATION PROVIDED IN SITE RED BY J.D BARNES DATED FEB 2, 2023
PGRADE EX. 5 IPE SLOPE ME RVEY PREPAI	525mm DIA. SEWER TO 750mm DIA. EASURED FROM INVERT INFORMATION PROVIDED IN SITE RED BY J.D BARNES DATED FEB 2, 2023
PGRADE EX. 5 IPE SLOPE AS OVIDED IN SI D PROPOSED RVICING & ST	525mm DIA. SEWER TO 750mm DIA. SSUMED BASED ON MEASURED FROM INVERT INFORMATION TE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023, INVERT ELEVATION IN a.m candaras associates inc. "SITE ORM WATER MANAGEMENT PLAN" DATED May 21, 2010

										STORM SEWE	R DESIGN SHEET										PREPARED BY: Z.B. CHECKED BY: K.K.
WSP CANADA INC.									11	01A, 1105, and 1163 I	KINGSTON ROAD -	PHASE 3									DATE: 25-Oct-23
										City o	f Pickering										LAST PRINTED: 25-Oct-23 FILE No 221-12931
											c .										
STREET	FROM M.H.	то М.Н.	CATCHMENT ID.	ha AREA Mixed/Use	R RUNOFF COEFFICIE	2.78 ENI A.R.	ACCUN 2.78 A.R.	M T <sub>c</sub> (MIN)	i RAINFALL INTENSIT (mm/hr	Q <sub>100</sub> - PEAK UNCONTROLLED FLOW Y (L/S)	Q <sub>CON</sub> CONTROLLED FLOW (L/S)	Q <sub>TOTAL</sub> Q <sub>100</sub> + Q <sub>CON</sub> (L/S)	PIPE DIA. ( mm )	SLOPE (%)	LENGTH (m)	CAPACITY (L/s)	VELOCITY (m/s)	TIME IN SECTION (min.)	TOTAL TIME (min.)	LOAD %	COMMENTS
Dhana d		OTMANUA	DUA	4.00	0.05	4.00	1.00	10.00	400.00	EAST	SITE	464.00	075	0.00	40.7	0.47.05	0.05	0.40	40.40	05%	
Phase 1	PHASE 1 SWM TANK	STM MH 1	PH 1	1.66	0.95	4.38	4.38	10.00	186.69	-	161.00	161.00	375	2.00	16.7	247.95	2.25	0.12	10.12	65%	
Phase 1	PHASE 1 PARK SUPERPIPE	E STM MH 1	PARK 1	0.10	0.25	0.07	0.07	10.00	186.69	-	10.30	10.30	450	-	-	-	-	-	-	-	- ALLOWABLE RELEASE RATE
Phase 1	STM MH 1	EX STM MH 10	-	-	-	-	4.45	10.12	185.49	-	171.30	171.30	450	0.50	10.3	201.60	1.27	0.14	10.26	85%	- PH1 + PH1 PARK ALLOWABLE RELEASE RATE
Phase 3	EX STM MH 10	EX STM MH 9	-	-	-	-	4.45	10.26	184.19	-	171.30	171.30	600	0.68	46.8	506.33	1.79	0.44	10.70	34%	- PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
Phase 3	STM MH 2	STM MH 6	ROW 1 + ROW 2	0.57	0.95	1.51	1.51	10.00	186.69	-	55.00	55.00	1050	0.00	174.4	0.00	0.00	-	-	-	PROPOSED FLAT 1050mm DIA. SUPERPIPE ACROSS SITE WITHIN PHASE 3     R.O.W. REFER TO SWM REPORT FOR MODELLING DETAILS     PHASE 2 & 3 ROW ALLOWABLE RELEASE RATE
Phase 3	STM MH 5	STM MH 6	PH 3	1.43	0.95	3.78	3.78	10.00	186.69	-	138.80	138.80	375	2.00	46.8	247.95	2.25	0.35	10.35	56%	- PH3 ALLOWABLE REALEASE RATE
Phase 3	STM MH 6	STM MH 8	-	-	-	-	0.00	10.35	183.36	-	193.80	193.80	1050	0.00	22.7	0.00	0.00	-	-	-	- PROPOSED FLAT 1050mm DIA. SUPERPIPE ACROSS SITE WITHIN PHASE 3 R.O.W. REFER TO SWM REPORT FOR MODELLING DETAILS
Phase 3	PHASE 3 PARK SUPERPIPE	STM MH 7	PARK 3	0.07	0.25	0.05	0.05	10.00	186.69	-	6.60	6.60	450	-	-	-	-	-	-	-	- SUPERPIPE WITH FLOW CONTROL
Phase 3	STM MH 7	STM MH 8	-	-	-	-	0.05	10.00	186.69	-	6.60	6.60	200	2.00	10.6	46.38	1.48	0.12	10.12	14%	- ALLOWABLE RELEASE RATE
Phase 3	STM MH 8	STM MH 9	-	-	-	-	0.05	10.00	186.69	-	200.40	200.40	1050	0.00	9.5	0.00	0.00	-	-	-	- PROPOSED FLAT 1050mm DIA. SUPERPIPE ACROSS SITE WITHIN PHASE 3 R.O.W. REFER TO SWM REPORT FOR MODELLING DETAILS
Existing Development	STM MH 9	EX STM MH 9	-	-	-	-	1.51	10.00	186.69	-	200.40	200.40	525	0.30	10.1	235.55	1.09	0.15	10.15	85%	
Existing Development	EX STM MH 9	EX STM MH 8 (OGS)	-	-	-	-	5.96	10.70	180.15		371.70	371.70	600	0.60	9.4	475.61	1.68	0.09	10.79	78%	<ul> <li>PIPE SLOPE AS PER a m candaras associates inc. "SITE SERVICING &amp; STORM WATER MANAGEMENT PLAN" DATED May 21, 2010. DESIGN INFO USED BECAUSE SURVEY CONTAINS CONFLICTING INFORMATION THROUGH THIS SEGMENT. SLOPE TO BE VERIFIED DURING DETAILED DESIGN.</li> </ul>
Existing Development	EX STM MH 8 (OGS)	EX STM MH 7	-	-	-	-	5.96	10.79	179.32	-	371.70	371.70	600	0.60	7.4	475.61	1.68	0.07	10.86	78%	<ul> <li>PIPE SLOPE AS PER a.m. candaras associates inc. "SITE SERVICING &amp; STORM WATER MANAGEMENT PLAN" DATED May 21, 2010. DESIGN INFO USED BECAUSE SURVEY CONTAINS CONFLICTING INFORMATION THROUGH THIS SEGMENT. SLOPE TO BE VERIFIED DURING DETAILED DESIGN.</li> </ul>
Existing Development	EX STM MH7	EX STM MH 6	-	-	-	-	5.96	10.86	178.66	-	371.70	371.70	600	0.39	51.1	383.45	1.36	0.63	11.49	97%	- PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
Existing Development	EX STM MH 6	Headwall	-	-	-	-	5.96	11.49	173.26	-	371.70	371.70	675	0.39	35.6	524.95	1.47	0.40	11.89	71%	- PIPE SLOPE UNKNOWN, ASSUMED SAME SLOPE AS UPSTREAM PIPE. SLOPE TO BE VERIFIED DURING DETAILED DESIGN.
										SOUTH	SITE										
PHASE 2	PHASE 2 SWM TANK	STM MH 3	PH 2	1.24	0.87	3.00	3.00	10.00	186.69	-	120.70	120.70	375	2.00	18.2	247.95	2.25	0.14	10.14	49%	- PH2 ALLOWABLE REALEASE RATE
PHASE 2	STM MH 3	EX STM MH 23	-	-	-	-	3.00	10.14	185.38	-	120.70	120.70	375	1.00	19.8	175.33	1.59	0.21	10.34	69%	
Existing Development	EX STM MH 20	EX STM MH 23	EX. 2	0.28	1.00	0.78	0.78	10.00	186.69	145.32	0.00	145.32	525	0.35	31.2	254.43	1.18	0.44	10.44	57%	- REFER TO EX. 2 IN PHASE 2 STORM DRAINAGE PLAN - PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
Existing Development	EX BUILDING	EX STM MH 23	EX. 4	1.01	1.00	2.81	2.81	10.00	186.69	-	43.40	43.40	250	2.00	21.0	84.10	1.71	0.20	10.20	52%	REFER TO EX. 4 IN PHASE 2 STORM DRAINAGE PLAN.     CONTROLLED RELEASE RATE AS PER a.m candaras associates inc. "SITE     SERVICING & STORM WATER MANAGEMENT PLAN" DATED May 21, 2010.
Existing Development	EX STM MH 23	EX STM MH 19	EX. 3	0.10	0.80	0.22	1.00	10.44	182.47	182.62	164.10	346.72	675	0.29	88.8	452.67	1.26	1.17	11.61	77%	- REFER TO EX. 3 IN PHASE 2 STORM DRAINAGE PLAN. - UPORADE EX. 525mm DIA. SEWER TO 675mm DIA. - PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
Existing Development	EX STM MH 19	EX STM MH 18	EX. 5	0.31	0.90	0.78	1.78	11.61	172.25	5 305.99	164.10	470.09	750	0.23	83.3	533.91	1.21	1.15	12.76	88%	- REFER TO EX. 5 IN PHASE 2 STORM DRAINAGE PLAN. - UPGRADE EX. 525mm DIA. SEWER TO 750mm DIA. - PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
Existing Development	EX STM MH 18	EX STM MH 17	-	-	-	-	1.78	12.76	163.34	290.16	164.10	454.26	750	0.30	13.3	609.77	1.38	0.16	12.92	74%	- UPGRADE EX. 525mm DIA. SEWER TO 750mm DIA. - PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
Existing Development	EX STM MH 17	BOX CULVERT	-	-	-	-	1.78	12.92	162.17	360.11	164.10	454.26	750	0.39	-	695.24	1.57	-	-	65%	UPGRADE EX. 525mm DIA. SEWER TO 750mm DIA.     PIPE SLOPE ASSUMED BASED ON MEASURED FROM INVERT INFORMATION     PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023,     AND PROPOSED INVERT ELEVATION IN a.m candaras associates inc. "SITE     SERVICING & STORM WATER MANAGEMENT PLAN" DATED May 21, 2010
*i <sub>100</sub> =2096.425/(T <sub>c</sub> +6.485)*0.863 RUNOFF COEFFICIENTS	NOTE: UNCONTROLLED RU	JNOFF COEFFICI	ENTS ARE SCALI	ED BY FA	ACTOR OF 1.2	25 (TO N	IAX VAL	LUE OF 1	) AS PE	R PICKERING STAN	DARDS			0.00							75
0.50 GREEN ROOF						0.9	5	IMPERV	IOUS RO	OF				0.90						1	<del>7</del>

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										STORM SEW	ER DESIGN SHEET										PREPARED BY:         Z.B.           CHECKED BY:         K.K.
WSP CANADA INC.									1	1101A, 1105, and 1163	KINGSTON ROAD	PHASE 4									DATE: 25-Oct-23
										City	of Pickering										LAST PRINTED:         25-Oct-23           FILE №         221-12931
STREET	FROM	то	CATCHMENT	ha AREA		2.78	ACCUN	T <sub>c</sub>	i RAINEA			Q <sub>TOTAL</sub>	PIPE	SLOPE	LENGTH	CAPACITY		TIME IN SECTION	TOTAL		COMMENTS
	М.Н.	M.H.					A.R.	( MIN )	INTENS	SITY (L/S)	(L/S)	(L/S)	( mm )	(%)	(m)	(L/s)	(m/s)	( min. )	( min. )	%	
				Mixed/Use					( mm / i	EAS1	I SITE										
Phase 1	PHASE 1 SWM TANK	STM MH 1	PH 1	1.66	0.95	4.38	4.38	10.00	186.6	69 -	161.00	161.00	375	2.00	16.7	247.95	2.25	0.12	10.12	65%	- PH1 ALLOWABLE REALEASE RATE
Phase 1	PHASE 1 PARK SUPERPIPE	STM MH 1	PARK 1	0.10	0.25	0.07	0.07	10.00	186.6	69 -	10.30	10.30	450	-	-	-	-	-	-		
																					- ALLOWABLE RELEASE RATE
Phase 1	STM MH 1	EX STM MH 10	-	-	-	-	4.45	10.12	185.4	49 -	171.30	171.30	450	0.50	10.3	201.60	1.27	0.14	10.26	85%	- PH1 + PH1 PARK ALLOWABLE RELEASE RATE
Existing Development	EX STM MH 10	EX STM MH 9	-	-	-	-	4.45	10.26	<b>184</b> .1	19 -	171.30	171.30	600	0.68	46.8	506.33	1.79	0.44	10.70	34%	- PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
																					PROPOSED FLAT 1050mm DIA SUPERPIPE ACROSS SITE WITHIN PHASE 3
Phase 3	STM MH 2	STM MH 6	ROW 1 + ROW 2	0.16	0.95	0.42	0.42	10.00	186.6	69 -	55.00	55.00	1050	0.00	174.4	0.00	0.00	-	-	-	R.O.W. REFER TO SWM REPORT FOR MODELLING DETAILS - PHASE 2 & 3 ROW ALLOWABLE RELEASE RATE
Phase 3	STM MH 5	STM MH 6	PH 3	1.43	0.95	3.78	3.78	10.00	186.6	69 -	138.80	138.80	375	2.00	46.8	247.95	2.25	0.35	10.35	56%	- PH3 ALLOWABLE REALEASE RATE
																					- PROPOSED FLAT 1050mm DIA. SUPERPIPE ACROSS SITE WITHIN PHASE 3
Phase 3	STM MH 6	STM MH 8	-	-	-	-	0.00	10.35	183.3	36 -	193.80	193.80	1050	0.00	22.7	0.00	0.00	-	-	-	R.O.W. REFER TO SWM REPORT FOR MODELLING DETAILS
Phase 3	PHASE 3 PARK SUPERPIPE	STM MH 7	PARK 3	0.07	0.25	0.05	0.05	10.00	186.6	69 -	6.60	6.60	450	-	-	-	-	-	-	-	- ALLOWABLE RELEASE RATE
Phase 3	STM MH 7	STM MH 8	-	-	-	-	0.05	10.00	186.6	69 -	6.60	6.60	200	2.00	10.6	46.38	1.48	0.12	10.12	14%	
Phase 3	STM MH 8	STM MH 9	-	-	-	-	0.05	10.00	186.6	69 -	200.40	200.40	1050	0.00	9.5	0.00	0.00	-	-	-	R.O.W. REFER TO SWM REPORT FOR MODELLING DETAILS
Phase 4	STM MH9	EX STM MH 9	-	-	-	-	0.42	10.00	186.6	69 -	200.40	200.40	525	0.30	10.1	235.55	1.09	0.15	10.15	85%	
Phase 4	EX STM MH 9	EX STM MH 8	-	-	-	-	4.88	10.70	180.1	15 -	371.70	371.70	600	0.60	9.4	475.61	1.68	0.09	10.79	78%	- PIPE SLOPE AS PER a.m candaras associates inc. "SITE SERVICING & STORM WATER MANAGEMENT PLAN" DATED May 21, 2010. DESIGN INFO USED DECAUSE CURPTER CONTAINED INFORMATION TURDINGLIGHT
		(OGS)								-										-	SEGMENT. SLOPE TO BE VERIFIED DURING DETAILED DESIGN.
Dhara 4							4.00	40.70	470 0	22	074 70	074 70	<b>COO</b>	0.00	7.4	475.04	4.00	0.07	10.00	700/	- PIPE SLOPE AS PER a.m candaras associates inc. "SITE SERVICING & STORM WATER MANAGEMENT PLAN" DATED May 21, 2010. DESIGN INFO USED
Phase 4	EX STM MH 8 (OGS)	EX STM MH 7	-	-	-	-	4.88	10.79	179.3	32 -	371.70	3/1./0	600	0.60	7.4	475.01	1.08	0.07	10.86	78%	BECAUSE SURVEY CONTAINS CONFLICTING INFORMATION THROUGH THIS SEGMENT. SLOPE TO BE VERIFIED DURING DETAILED DESIGN.
Phase 4	EX STM MH7	EX STM MH 6	_				4 88	10.86	178 6	66 -	371 70	371.70	600	0.39	51.1	383 45	1.36	0.63	11 49	97%	- PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE
																					SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
Phase 4	EX STM MH 6	Headwall	-	-	-	-	4.88	11.49	173.2	26 -	371.70	371.70	675	0.39	35.6	524.95	1.47	0.40	11.89	71%	- PIPE SLOPE UNKNOWN, ASSUMED SAME SLOPE AS UPSTREAM PIPE. SLOPE TO BE VERIFIED DURING DETAILED DESIGN.
Phase 2	PHASE 2 SWM TANK	STM MH 3	PH 2	1.24	0.87	3.00	3.00	10.00	186.6	50UT 69 -	H SITE 120.70	120.70	375	2.00	18.2	247.95	2.25	0.14	10.14	49%	- PH2 ALLOWABLE REALEASE RATE
Phase 2	STM MH 3	EX STM MH 23	-	-	-	-	3.00	10.14	185.3	38 -	120.70	120.70	375	1.00	19.8	175.33	1.59	0.21	10.34	69%	
Phase 4	EX STM MH 23	EX STM MH 19	PH4 D1	0.19	0.68	0.36	0.36	10.34	183.4	41 65.39	120.70	186.09	675	0.29	88.8	452.67	1.26	1.17	11.51	41%	VEREAL OF THE DT IN PRASE 4 STORM DRAINAGE FLAN     UPGRADE EX. 525mm DIA. SEWER TO 675mm DIA.     JIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE
																					SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
Phase 4	PHASE 4 SWM TANK	EX STM MH 19	PH 4	1.36	1.00	-	-	10.00	186.6	69 -	131.70	131.70	375	2.00	13.9	247.95	2.25	0.10	10.10	53%	- PH4 ALLOWABLE REALEASE RATE
																					- REFER TO PH4 D2 IN PHASE 4 STORM DRAINAGE PLAN.
Phase 4	EX STM MH 19	EX STM MH 18	PH4 D2	0.19	0.65	0.34	0.70	11.51	173.0	08 121.13	252.40	373.53	750	0.23	83.3	533.91	1.21	1.15	12.66	70%	- UPGRADE EX. 525mm DIA. SEWER TO 750mm DIA. - PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE SUBJECT DEPADED BY I.D. PADRIES DATED EEP. 2, 2022
																					SURVET PREPARED BT J.D DARIVES DATED FED 2, 2023
																					- UPGRADE EX. 525mm DIA. SEWER TO 750mm DIA.
Phase 4	EX STM MH 18	EX STM MH 17	-	-	-	-	0.70	12.66	164.0	08 114.83	252.40	367.23	750	0.30	13.3	609.77	1.38	0.16	12.82	60%	- PIPE SLOPE MEASURED FROM INVERT INFORMATION PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023
		EV OTHER AT	DADK (	0.00	0.05		0.00	40.00	400.0												- SUPERPIPE WITH FLOW CONTROL
Phase 4	PHASE 4 PARK SUPERPIPE	EX STM MH 17	PARK 4	0.23	0.25	-	0.00	10.00	186.6	69 -	22.60	22.60	600	-	-	-	-	-	-	-	- ALLOWABLE RELEASE RATE
rnase 4	51 M MH 10	EASIMINH 1/	-	-	-	-	0.00	10.00	186.6	-	22.00	22.00	200	2.00	24.3	40.38	1.48	0.27	10.27	49%	
																					- UPGRADE EX. 525mm DIA. SEWER TO 750mm DIA. - PIPE SLOPE ASSUMED BASED ON MEASURED FROM INVERT INFORMATION
Phase 4	EX STM MH 17	BOX CULVERT	-	-	-	-	0.70	12.82	162.9	90 114.01	275.00	367.23	750	0.39	-	695.24	1.57	-	-	53%	PROVIDED IN SITE SURVEY PREPARED BY J.D BARNES DATED FEB 2, 2023, AND PROPOSED INVERT ELEVATION IN a.m candaras associates inc. "SITE SERVICING
				1				1													& STORM WATER MANAGEMENT PLAN" DATED May 21, 2010
*i -2006 425//T +6 495/40 962						(TO 144	V \/A1 ·														
1100-2090.420/(1 <sub>c</sub> +0.480) <sup>w</sup> 0.803	NOTE: UNCONTROLLED RUN	NOFF COEFFICIE	IN IS ARE SUALE	U BY FA	GTUR UF 1.25	(10 MA	v ALL		) AS PE	ER PIUNERING STANL	JARUS										
RUNOFF COEFFICIENTS																					
						0.05				TOPADE				0.00							

SOFT LANDSCAPING/PARK GREEN ROOF 0.95 IMPERVIOUS AT GRADE 0.95 IMPERVIOUS ROOF 0.90 0.90 No. OF SHEETS 1 0.25













![](_page_67_Figure_0.jpeg)

![](_page_68_Figure_0.jpeg)

![](_page_69_Figure_0.jpeg)

![](_page_70_Figure_0.jpeg)

![](_page_71_Picture_0.jpeg)

![](_page_71_Picture_1.jpeg)










## SUPPORTING DOCUMENTS

SEWE	R IN	IVER1		TA TA		NOTES	мн/св	DIRECTION	DIAMETER	INVERT	TOP OF LID/ GRATE FIFV		NOTES	
CB#1	N	200	1.31	85.54	84.23		STM MH#7	N SE	600 600	2.30 2.33	84.89	82.59 82.56		
CB#2	SE	200	1.23	85.54	84.31		STM MH#8 STM	NW S N	<i>*600</i> <i>*600</i> 600	$\pm 2.50$ $\pm 2.50$ 2.30	84.99 84.98	±82.49 ±82.49 82.68 82.65	OIL GRIT SEPARATOR	
СВ#4	N	300	1.25	84.89	83.52		MH#9 STM MH#10	SE SW NW N NE	300 300 450 450	2.33 1.94 1.92 N/A 1.94	85.06	83.04 83.14 N/A 83.12	1.95TO DEBRIS	
CB#5	NE	300	1.09	84.95	83.86		STM MH#11	S E W	<i>*150</i> 300 300	<i>*2.06</i> 1.90 1.84	85.06	* <i>83.00</i> 83.16 83.22	REDUCED PIPE	
DCB#6	NE	300	1.26	84.32	83.06		STM MH#12	N E SW N	450 300 450 450	2.34 ±2.07 ±2.02 2.65	85.86 86.13	83.52 ±83.79 ±83.84 83.48		
DCB#7 CB#8	SE w	300	1.17	84.28	83.11		STM MH#13 STM	NE S SW	450 450 150	2.70 2.62 1.80 2.19	85.51	83.43 83.51 84.33 83.32		
CB#9	w	250	1.30	84.91	83.61		STM MH#15	SW N NE	450 450 <i>*450</i> 450	2.17 1.83 1.74 1.85	85.56	83.34 83.73 83.82 83.71	NE-RECESSED	
CB#10	w	300	1.43	85.38	83.95		STM MH#16	NW N SE	300 150 450	1.40 1.31 2.15	86.32	84.92 85.01 84.17		
CB#11	S	450	1.52	85.24	83.72		STM MH#17	*N NE *S	*525 *525 *525	N/A 2.00 N/A	84.02	N/A 82.02 N/A	OIL GRIT SEPARATOR	_
CB#12	SE NW	300 450	1.30	85.41 85.62	84.11		STM MH#18	NE SW NW	250 525 250 525	1.97 1.98 3.75	84.04 86.18	82.07 82.06 82.43 82.28	NE-W/ ORIFICE PIPE	
CB#14	S NW	450 250	1.86	85.26	83.76 84.19		мн#19 STM MH#20	NW NW NE SE	450 300 525	2.19 1.84 2.20	84.88	82.26 82.69 83.04 82.68		
CB#15	NE	250	0.96	85.44	84.48		STM MH#21	SW NE SE SW	250 250 250 250	2.17 1.36 1.15 1.40	84.48	82.71 83.12 83.33 83.08		
CB#16	SE	300	0.78	85.71	84.93		STM MH#22	NW SE	100 600	2.08 2.10	84.54	82.46 82.44	NW-REDUCED PIPE	_
CB#17	SE SW	300 250 250	1.29 1.27	85.65	84.36 84.38 84.34		STM MH#23 STM	NW SW NF	525 525 450	4.70 4.73 2.20 2.18	87.27 85.15	82.57 82.54 82.95 82.95		
CB#19	SSE	250	1.44	84.69	83.25		мн#24 STM MH#25		450 450 100 450	2.18 2.22 1.57 1.76 1.62	85.16	82.93 83.59 83.40 83.54		
CB#20	SE	250	1.49	84.81	83.32		STM MH#26	S *S	450 *250	1.87 N/A	N/A	83.29 N/A	UNABLE TO ACCESS	
CB#21	SE	250	1.58	84.77	83.19		STM MH#27	NW NE	300 450	2.31 ±2.32	86.26	83.95 ±83.94		
CB#22	*NW NW	*250 250	N/A 1.30 1 31	84.19 84.19	N/A 82.89	PARKED TRUCK	STM MH#28 STM	NE SW	450 450 450	1.87 1.88 1.60	84.94	84.12 84.11 83.34		
, CB#24	SE	250 250	1.30 N/A	N/A	82.89 N/A	1.10 TO DEBRIS	мн#29 STM MH#30	SW NW E	450 450 300 450	1.62 1.03 1.06 1.10	84.98	83.32 83.95 83.92 83.88		
DCB#25	SW	300	1.35	84.88	83.53		STM MH#31	NW SE	450 450	1.14 1.20	85.17	84.03 83.97		JR-16
CB#26	NW NE SE W	450 150 450 250	2.14 1.71 2.15 1.88	85.03	82.89 83.32 82.88 83.15		STM MH#32	*N *SW	*250 *250	N/A N/A	86.72	N/A N/A	BOLTED SHUT	R/W
CB#27 CB#28	N/A SW	N/A 250	N/A 1.20	84.77	N/A 83.24	NO PIPE	MH#1 SAN MH#2	NE SW NW NW'	1050 1050 150 150	5.80 5.77 1.37 2.62	85.10	79.30 79.33 83.69 82.44	NW'-DROP	
DCB#29	SE	250	1.24	84.83	83.59		SAN MH#3	SE SE W	200 150 150	2.63 2.81 2.77	84.50	82.43 81.69 81.73		PART 1, PLAN 40R-16455
СВ#30	SE SW	250 450	1.27 1.32	84.74	83.47 83.42		SAN MH#4	NW NE SW	200 1050 1050	4.38 5.13 5.10	84.29	79.91 79.16 79.19		
CB#31	NW	250	1.14	84.95	83.81		SAN MH#5 SAN	N SE	200 200	4.23 4.25	84.45	80.22 80.20		
CB#32 CB#33	W	300 300	1.57	85.53 85.24	83.96		MH#6 SAN MH#7	NW S N NE	200 200 200 200	4.07 4.22 3.56 3.40	84.53	80.46 80.31 81.38 81.54		
DCB#34	NW	250	1.0	84.77	83.77		SAN MH#8	SE NW NE S	200 150 200 200	3.60 2.74 3.02 3.04 2.97	85.06	81.34 82.32 82.04 82.02 82.09		PART 6, PLAN 40R-16455
DCB#35	NW	250	0.70	84.84	84.14		SAN MH#9	NE SW	150 150	3.09 3.08	85.23	82.14 82.09		PART 2, PLAN 40R-16455
DCB#36	W	300	0.72	84.78	84.06		SAN MH#10 SAN	SE W	150 150 150	2.00 1.98 2.17	85.29 85.94	83.29 83.31 83.77		PART 3, PLAN 40R-16455 PART 7, PLAN- 40R-16455
CB#38	*E	∠əu *250	*1.50	*85.25	04.06 *83.75		MH#11 SAN MH#12	SW N S	150 200 200	2.10 2.07 1.96	87.91	83.84 85.84 85.95		PART 4, PLAN 40R-16455
CB#39	*NE	*250	*1.50	*85.25	*83.75		SAN MH#13	NE SW	*1050 *1050	6.50 6.40	85.27	78.77 78.87	W/ PLATFORM	
STM MH#1	NW NE SW	450 525 400 825	1.87 1.97 1.90 2 27	85.77	83.90 83.80 83.87 82.77		SAN MH#14	NE SW	200 200 <i>*150</i>	1.81 2.30 <i>*3.95</i>	84.91 * <i>±86.56</i>	83.10 82.61 *±82.61		PART 8,
MH#2 STM	E W NE SW	825 300 825 <i>*900</i>	2.44 1.90 2.38 <i>*2.37</i>	84.82	82.60 83.14 82.44 82.45		SAN MH#15 SAN	*NW *NE *SW	*150 *1050 *1050 *200	*6.54 *7.41 *7.41 *2.90	*86.80	*±79.02 *±79.15 *±79.15 *83.90	UNABLE TO	- - - - - - - - - - - - - - - - - - -
STM MH#4	W NW E SW	*525 600 900 900	<i>*2.33</i> ±1.98 2.34 2.14	84.41	82.49 ±82.43 82.07 82.27		SAN MH#17	*3 *SE	*200	*2.30 N/A	N/A	+04.3U N/A	UNABLE TO FOUND	
STM MH#5	NW SE	600 100	2.26 2.29	84.76	82.50 82.47	SE - REDUCED PIPE	MH#1	NW SE	±1000 ±1000	2.50 2.50	86.34	83.84 83.84	POSSIBLY STORM MANHOLE	
STM MH#6 <i>*INFORMATI</i>	NW S	600 675	2.23 2.26	84.59	82.36 82.33 <i>REGION_OF_DURH</i>	IAM	MH#2 <i>*INF.ORM/</i>	NW SE	±1000 ±1000	2.90 2.92 <i>RECORDS</i>	85.62	82.72 82.70 <i>REGION OF DURI</i>	POSSIBLY STORM MANHOLE	
AND CITY (	OF PICKEI	RING; NOT F	IELD VERIF	IED BY ONSIT	E LOCATES INC.		AND CIT	Y OF PICKE. 	RING; NOT I	IELD VERIF	 	E LOCATES INC.		-1191
							/		~		/			LOT 24, $4$
							/		-011	)	/			PART 1. PLAN 40R-12678
							/		_	/				PIN 26317 -0070
							/	D 75		/				331025
						, 		A AN		/				Ď N V
						/		STC STC	/	1				572, F
						/		LV LC	/					D2885
						/	SC	26317	/					
						/	$\sum_{CE} A$	٠V	 					57'20"W
							0 MAN	/	1					, AS
							ALL,	/			- <i>i</i>	() <b>A</b> • ·		S. T.E.
				PA	ART 2, F 40R-11⊿	, PLAN- 83 ~ ~	740	/		- PAR 4C	1, P )R-1148	'LAN 83		
				(	(P1,P5&SET) R (MEAS) A	2=18.50 =28.02	-	/ \ /				PIN SUB	BJECT TO	26317 EASEMENT AND RIGHT-OF-WAY AS IN D331029
				(P1,	(P1,P5) / (MEAS) <b>C</b> (P1,P5) ( P5&MEAS) <b>N8</b>	a=28.08 2=25.42 C=25.46 •31′15″E	/ \		CURB		N58:02'40"	( <u>P</u> 9)	PART (rpe)	8, PLAN 40R-12678
					/		X	4500 _CE			27.39′30' 27.39(P1,	∟ (Р1,́Р5&МЕ, ,Р5,Р9&МЕАЅ с	AS)	Signal         San MH#17 (APPROX.LOC.; POSS. BURIED)         N56*06'15"E (P1,P5&MEAS)           G         G         G         G
					/ N44* / (P5/	C=5.07 08'00''E &MEAS)	$\langle \rangle$	ST 200	WV LING		♦ W = 200¢	100¢ WS	6.2₩ <u> </u>	
					/ <u>N5</u>	4.94 1°46'25"E	40			SAN	EDGE BC 0.7 S	STM		OF LS
				/	· (P1, /	BACK OF	IB (RP (RPE)	е)св #1241			EDGE BACK			$\frac{1}{26317} \xrightarrow{\text{SAN}} \frac{1}{26317} \xrightarrow{\text{SAN}} \frac{1}{26317} \xrightarrow{\text{SAN}} \frac{1}{84.89} \text{ OF}$
				/	F CC	ENCE RNER 0.1 N 0.8 E SSIB	FUU	×	PED 1.2 N			UT	UT	_ABANDONED
								$\sim L$		$\mathbf{n}$	CHAIŃ	N57 <b>*</b> 59'3	0"E (P1,P5&M	IEAS)

•**39′00″E**(CALC1&MEAS

S.T.E. AS IN C0144390

`♠ SCP 00919680467

PART 6, PLAN-40R-6179 *s.t.e. as in-c0144390* 

40R-25448 Ó EASEMENT AS IN D288571, D338631, D347349 AND DR746227 -SUBJECT \_\_\_\_\_PART 47, PLAN 40R-25448

PLAN



PLOTTED: 2/2/2023

G: \22-25-073\00\22-25-073-00.dgn



