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PROPOSED REDEVELOPMENT 1755 & 1805 Pickering Parkway, City of Pickering, Ontario

## FUNCTIONAL SERVICING AND STORM WATER MANAGEMENT REPORT

### (PHASE 1)

Prepared For:

Pickering Ridge Lands Inc. & Bayfield Realty Advisors

ORIGINAL: March 18, 2022 REVISED: April 20, 2022 (for Submission)

\* Please refer to the Master Servicing Study prepared by Odan Detech Group dated April 13th, 2022 for details on the ultimate development.

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#### TABLE OF CONTENTS

#### DESCRIPTION

#### Page

1.		1
2.	SCOPE OF WORK	3
3.	SANITARY SERVICING	4
4.	WATER SUPPLY AND DISTRIBUTION	12
5.	STORMWATER MANAGEMENT & FOUNDATION WATERPROOFING	17
6.	WATER BALANCE	31
7.	WATER QUALITY	33
8.	GRADING CONSIDERATIONS	34
9.	EROSION AND SEDIMENT CONTROL	34
10.	SOILS REPORT AND HYDROGEOLOGY:	34
11.	RECOMMENDATIONS:	35
12.	CONCLUSIONS	35
13.	REFERENCES	36

#### LIST OF FIGURES

Exhibit 1 Location of the project site	2
Exhibit 2 Full build out layout and location of Phase 1	2
Exhibit 3 Durham Region layout of existing sanitary sewers	5
Exhibit 4 - Region Map 1 North [1899 Brock Rd & Mixed-use Lands]	6
Exhibit 5 – Region Map 1 South [Subject site and 1731/1735 Pickering Pkwy]	7
Exhibit 6 – Region Map 2 South [Metropia Lands]	7
Exhibit 7 Durham Region layout of existing water system	15
Exhibit 8 - City layout of existing Storm sewers and Site sewers	18
Exhibit 9- XPSWMM PHASE 1 MODEL WITH NODE LABELS	23
Exhibit 10- XPSWMM PHASE 1 MODEL WITH TRIBUTARY AREAS	24
Exhibit 11- XPSWMM profile plot STM TANK to EXMH5 – 100-YR Chicago	25
Exhibit 12- XPSWMM profile plot STM TANK to EXMH5 – 5-YR Chicago	26

#### LIST OF TABLES

Table 1 – Proposed population and sanitary peak flow estimate (Phase 1)   Table 2 – Offsite sewer improvements	10 11
Table 3 – Allowable pressures	13
Table 4 – Total Water Demand For Phase 1 – First Pickering Place	14
Table 5 – Comparison Existing flows to Phase 1 – Out pipe at EX.MHS3	21
Table 6 – Target Peak Flows from Phase 1 site (allowable)	21
Table 7 – Proposed XPSWMM model hydrology parameters	28
Table 8 – Peak Flows from Phase 1 Site	29
Table 9 – SWMM Quantity Features for Phase 1	29
Table 10 – Summary Information for Proposed Re-Development	35

#### **APPENDIX A**

Aerial Photo of Existing Site Phase 1 Site Plan of the Proposed Development (reduced) Ultimate Site Plan of the Proposed Development (reduced)

#### APPENDIX B

Redeveloped site Phase 1 sanitary sewer design sheet

Redeveloped sites (subject site, 1899 Brock Road and surrounding tributaries) sanitary sewer design sheet

#### APPENDIX C

FUS Fire Demand Calculations Location of hydrant flow tests Hydrant flow tests

#### **APPENDIX D**

XPSWMM models and output upon request Water Balance Calculations

#### APPENDIX E

- Figure 1 Preliminary Site Servicing Plan
- Figure 2 Preliminary Grading Plan
- Figure 3 Post Development Watermain Service
- Figure 4 Post Development Storm Service
- Figure 5a Post Development Sanitary Service
- Figure 5b Post Development Sanitary Service
- Figure 6 Post Sanitary Tributary Area Plan
- Figure 7 Pre Development Storm Tributary Area Plan
- Figure 8 Post Development Storm Tributary Area Plan

Figure 9 – Notion Road – Profile

- Figure 10 Pickering Parkway Profile 1/2
- Figure 11 Pickering Parkway Profile 2/2

#### 1. INTRODUCTION

#### Site Description

The subject development comprises Phase 1 of a multi phased development, phase 1 has an area of 1.18 ha and is bound by existing commercial lands to the north, Highway 401 to the south, existing commercial lands to the east and Brock Road to the west.

Please refer to the Master Servicing Study prepared by Odan Detech Group dated January 25<sup>th</sup>, 2022 for details on the ultimate build out future development.

Currently, the site is developed with multi-tenant, "big box" and smaller commercial retail establishments with associated asphalt parking lots. The topography of the site is relatively flat sloping northeast. The subject site known as First Pickering Place (FPP) is currently designated as "Mixed Use Areas – Specialty Retailing Node" in the Pickering Official Plan; the lands with this designation are intended to have the widest variety of uses and highest levels of activities. An aerial view of the site can be found in Appendix A showing surrounding uses. Refer to Exhibit 1 below for the site location. Exhibit 2 shows the plan of the redeveloped site and location of phase 1 within the site.

#### Background

This report will evaluate the serviceability of the proposed Phase 1 redevelopment with respect to sanitary, water, and storm servicing. This report will also evaluate the stormwater management (SWM) strategy to meet the SWM requirements set out by regulatory agencies.



Exhibit 1 Location of the project site



Exhibit 2 Full build out layout and location of Phase 1

#### 2. SCOPE OF WORK

The Odan/Detech Group Inc. was retained by the owners, **Pickering Ridge Lands Inc. & Bayfield Realty Advisors** to propose a servicing scheme(s) for the Redevelopment of 1755 & 1805 Pickering Parkway (Pickering Design Centre). The scope of work in brief involves the following:

- a) Gather information on the existing services for the Site and surrounding the Site.
- b) Work with or assemble a team of Consultants and Vendors to perform specialized tasks required for the global servicing assessment.
- c) Meetings/conversations with consulting team and land owners in order to coordinate developments.
- d) Produce Servicing Schemes that will allow for the development of the intensified site at full build out and focus on the development of Phase 1. The servicing analysis entails a review for sanitary waste water, water distribution, storm water management and grading.

Currently, the proposed development area is divided into 7 blocks (Block '1' to Block '7'), of which Phase 1 corresponds to Block '1'. The proposed redevelopment in Phase 1 will consist of a mixed-use development with two towers of 31 storeys. The proposed building will have retail at grade, 630 apartment dwelling units, 4 level of underground parking and surface parking, and 1,538 m2 of indoor and 1,052 m2 of outdoor amenity space. Refer to site plan prepared by Turner Fleischer Architects Inc. in Appendix A for additional information.

#### 3. SANITARY SERVICING

#### **Existing Sanitary Sewer Infrastructure**

As-constructed and design drawings obtained from the Region of Durham and the City of Pickering show that an existing 250 mm diameter sanitary sewer in Pickering Parkway are located as the main sanitary outlet of the subject site.

There are two existing sanitary sewer connections to the site, a 250mm sanitary outlet toward Pickering Parkway at the north of the site and a 150 mm sanitary outlet toward Notion Road at the east of the site.

Refer to Exhibit 3 for the location of the Site and the layout of the existing sanitary sewers in the area.

The majority of sanitary flow from the existing commercial site is conveyed through an existing 250 mm diameter sanitary sewer west to east along Pickering Parkway. Then connected to a 250 mm diameter sanitary sewer at the intersection with Marshcourt Dr, which conveys the sanitary flow to the north. The 250 mm diameter sanitary sewer on Marshcourt Dr then increases to a 375 mm diameter sewer at the Region's easement and the sanitary sewer conveys the collected sanitary flow to a 375 mm diameter sanitary sewer on Notion Road. The 375 mm diameter sanitary sewer on Notion Road is connected to a 750 mm sanitary sewer on Orchard Road that conveys the collected flow to the east. The 750mm pipe is the outlet for the subject site. The sanitary analysis will be conducted considering the flow from all sites that presently flow to Orchard Road and the future flow from the redevelopment of 1899 Brock Road.

In completing the analysis, the following information will be used or relied upon:

- Drawings from City of Pickering.
- Drawings from The Regional Municipality of Durham.
- Sanitary system Maps from The Regional Municipality of Durham
- Design guidelines for sanitary sewers systems from The Regional Municipality of Durham
- Master Servicing & Stormwater Management Report -1899 Brock Road, SCHAEFFERS Consulting Engineers, May 2021
- Functional Servicing & Stormwater Management Report Residential Townhouse Development 1856 Notion Road, GHD, Jan 2018

#### EXISTING SYSTEM REVIEW

Based on findings in the MSS report by Odan Detech, the redeveloped site cannot be routed through the existing sewer system along Pickering Pkwy, Marshcourt Drive, easement between homes to Notion Road to Orchard Drive Due to limitations of the existing sanitary sewer capacity, it would mean replacing a relatively deep sewer between two existing homes. The recommended and preferred routing would be along Pickering Pkwy to Notion Road to Orchard Drive.

#### FIRST PICKERING PLACE FUNCTIONAL SERVICING AND STORM WATER MANAGEMENT REPORT PICKERING, ONTARIO



Exhibit 3 Durham Region layout of existing sanitary sewers

5

#### **REGION OF DURHAM PREFERRED SYSTEM**

Discussion with the Region of Durham (Aaron Christie) regarding the redevelopment of the subject site and that of the proposed future development lands can be summed up as follows:

- The Region solution for the intensification is to provide a sewage pump station (SP) on the south side of HWY 401. From this SP a large trunk sewer will be extended North under HWY 401 to Notion Road, then continue North on Notion Road. The design and EA for this project will start shortly.
- 2) Sanitary mapping has been provided by the Region which indicates proposed future development lands and the associated tributary areas which will ultimately discharge to the SP on the south side of HWY 401 via Pickering Parkway and the Notion Road trunk sewer. Population densities for these proposed development lands were provided by the Region. Refer to Exhibits 4, 5 & 6 below for the Region's sanitary mapping and related population densities.

#### Region of Durham Sanitary Maps & Correspondence indicating population densities



Exhibit 4 – Region Map 1 North [1899 Brock Rd & Mixed-use Lands]



Exhibit 5 – Region Map 1 South [Subject site and 1731/1735 Pickering Pkwy]



Exhibit 6 – Region Map 2 South [Metropia Lands]

- 3) The Region has allowed for the Phase 1 of 1899 Brock Road to be discharged west ward to Brock Road and will therefore not be included in our Phase 1 downstream sanitary analysis.
- 4) The Phase 1 for the subject site will be allowed to discharge to Orchard Drive North on Notion Road, for the interim condition.
- 5) In the full build out condition the temporary sewers on Notion Road will be replaced by the Region with a trunk sewer. Thus, all the sewage from the existing and redeveloped sites will flow south in the Notion Road trunk, under HWY 401 to the new Region SP.
- 6) The Region prefers that the Sewer to Notion Road along Pickering Parkway be installed to accommodate the fully built out sites and the existing sites along the way.
- The Region will allow a smaller sewer diameter pipe on Notion Road than on Pickering Parkway for the interim condition since the trunk sewer will replace this to flow South under the HWY 401.
- 8) The Region did not offer a real time table for the SP and Notion Road trunk sewer, however stated that it would be available for the Phase 2 of the development.

The Region has also given us the approximate reserve capacity of the Orchard Drive sewer from where we show it on Exhibit 3 eastward. See the following e-mail from Aaron Christie.

#### Hello Mark,

At this time base your study on the assumption that there could be up to a capacity of 150 l/s available within the 750mm sanitary sewer at Orchard Road. This is based on preliminary input received from the Region of Durham and is subject to change as your application and development of the surrounding lands moves forward.

Based on my interpretation of the mapping, the 600mm watermain on Brock Road has a 300mm dia. tee to the west and then there is a 300mm x 300mm dia. tee and 90 degree bend providing the 300mm dia. watermain to the east across Brock Road to Pickering Parkway.

Thanks,



Aaron Christie, P.Eng. | Manager, Engineering Planning & Studies Works Department The Regional Municipality of Durham <u>Aaron.Christie@durham.ca</u> | 905-668-7711 extension 3608 | <u>durham.ca</u> My pronouns are he/his



#### **Design Criteria**

Sanitary flows for the subject site are calculated based on the Regional Municipality of Durham design specifications for sanitary sewers. The summary is as follows:

#### **Residential**

- Average flow: 364 L/person/day
- Infiltration: 22.5 m<sup>3</sup> gross ha/day (0.26 l/s/ha/day) when foundation drains are not connected to the sanitary sewer.
- Peaking Factor:

$$K = 1 + \frac{14}{4 + P^{1/2}}$$

Where K=Harmon Peaking Factor, P = Population in thousands. K-Maximum= 3.8m, K-Minimum= 1.5

• When the number and type of housing units within a proposed development are known, the calculation of population for the proposed development shall be based on the following:

Type of Housing	Persons/ha
Single Family Dwelling,	60
Semi-detached & Duplex	100
Townhouses	125
Apartment(s)	
- Low density (62 u/ha)	150
- Medium to low density (86 u/ha)	210
- Medium density (124 u/ha)	300
- High Density (274 u/ha)	600
u/ha = units per hectare	

Туре	of	Housing
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Single Family Dwelling, Semi-Detached and Links	3.5	
Townhouses/Stacked Townhouses		
Apartment(s)		
- 1 Bedroom or smaller (Bachelor)	1.5	
- 2 Bedroom	2.5	
- 3 Bedroom	3.5	
- 4 Bedroom or larger	4.5	

#### **Commercial**

Design Flow: 180 m³/gross floor area ha/day (2.08 l/s/day) including infiltration and peaking effect.

Persons/Unit

#### EXISTING SANITARY SEWER CAPACITY CALCULATION

The capacity of the existing sanitary sewer system from the subject site to Orchard Rd was evaluated in the MSS report by Odan Detech. The existing sanitary sewer was found to have insufficient capacity to accept Phase 1 of the subject development. Refer to the MSS report by Odan Detech for further details and information pertaining to the existing sanitary capacity, including sanitary design spread sheet and existing sanitary tributary plan.

#### PROPOSED SANITARY SEWER DESIGN CONSIDERATION

Based on our discussion with the Region of Durham (Aaron Christie), that they (the Region) want the redeveloped flow from 1899 Brock Road and the updated tributary areas, provided by the Region, to flow from their Site east on Pickering Parkway to Notion Road.

Metropia is planning to develop a new townhouse development at 1856 Notion Road known as the Metropia Site. The details are contained within the "Functional Servicing and Stormwater Management Report", by GHD, Jan 2018. The sanitary flow (11.67 L/s) from the development will be routed to the existing manhole (MH35-6) on Pickering Parkway.

Since four existing retail buildings will remain operational within the site for phase one construction. The construction of new sewers will need to be phased to ensure drainage is maintained to the existing buildings.

Table 1 – Proposed population and sanitary peak flow estimate (Phase 1)							
Unit Type /Land Use	Number of Units /Gross floor Area	Persons/ Unit	Population	Peaking Factor	Infiltration (L/sec)	Sanitary Flow (L/sec)	
North Sanitary O	utlet to Pickering I	Parkway					
Commercial (Ex.)	1.78 ha	-	-	1	-	3.71	
Commercial (Prop.)	0.169 ha	-	-	1		0.35	
Apartments (Prop.)	630 Units	2.5	1,575	3.66	0.26	24.50	
Total	-	-	-	-		28.56	
East Sanitary Outlet to Notion Road							
Commercial (Ex.)	0.425 ha	-	0.425 ha	1		0.88	
Total							

Table 1 is a summary of the flows generated by the Site during Phase 1.

The total flow to the 750mm sanitary sewer outlet at Orchard Road for Phase 1 of the subject site including existing commercial is 85.62 L/sec. Refer to sanitary design sheets in Appendix B for detailed calculations of the Phase 1 development and the future ultimate build out development.

Existing sanitary flow into the Orchard Road outlet is 46.68 L/s (refer to MSS report by Odan Detech). Thus the increase in flow, 38.94 L/s, is less than the available excess flow capacity of 150 L/s (provided by Durham Region), therefore the outlet sewer has adequate capacity for Phase 1 of the subject development.

#### SUMMARY AND RECOMMENDATION

Based on the above review, analysis and findings of the MSS report by Odan Detech we offer the following summary and recommendations:

- Phase 1 of First Pickering Place cannot be accommodated by the existing sanitary sewer system and present routing path. This would mean replacing a deep sanitary sewer between two existing houses and is not recommended. Refer to MSS report for detailed analysis of the existing conditions.
- 2) The 750 mm sanitary sewer on Orchard Road has sufficient capacity to accommodate Phase 1 of First Pickering Place and the existing uses.
- 3) We recommend that the owners of First Pickering Place build the sanitary sewer on Pickering Parkway from 1899 Brock Road site to Notion Road to accommodate the full build out of all future development sites and the existing flows. This recommendation allows the Pickering Parkway sanitary sewer to be installed and completed at one time rather than removing the road surface on separate occasions during future phasing. This section of sanitary sewer will be subject to development charges as discussed with the Region of Durham.
- 4) The sanitary pipe on Notion Road (from Pickering Parkway to Orchard Rd) will be sized to convey existing flows and flows from Phase 1 (First Pickering Place) to the existing Orchard Road sanitary sewer. The Region will allow this interim condition at limited capacity until such time that the Ultimate Trunk Sewer is constructed in the future to convey flows to the South SP. The interim pipe will be downsized from that on Pickering Parkway, the Region will allow this, since it is a temporary measure until the Region replaces it with a trunk sewer on Notion Road.

Refer to sanitary design spreadsheets in Appendix B for detailed calculations of Phase 1 development and the Ultimate build out development.

Sewer location	Upstream MH	Downstream MH	Sewer size, length and slope	Comments
Pickering Parkway	1899 Brock Road	EX MH 34-82	525mm – 112m @ 1.0%	New pipe
Pickering Parkway	EX MH 34-82	Prop MH9A	675mm – 45m @ 0.37%	Replacement pipe
Pickering Parkway	Prop MH9A	EX MH 34-83	675mm – 45m @ 0.42%	Replacement pipe
Pickering Parkway	EX MH 34-83	EX MH 35-5	675mm – 100m @ 0.47%	Replacement pipe
Pickering Parkway	EX MH 35-5	EX MH 35-6	675mm – 100m @ 0.48%	Replacement pipe
Pickering Parkway	EX MH 36-6	EX MH 36-7	750mm – 83m @ 0.38%	Replacement pipe
Pickering Parkway	EX MH 36-7	EX MH 36-8	750mm – 80m @ 0.46%	Replacement pipe
Pickering Parkway	EX MH 35-8	EX MH 35-28	750mm – 101m @ 0.57%	Replacement pipe
Notion Road	EX MH 35-28	Prop MH 13A	375mm – 15m @ 0.22%	New pipe
Notion Road	Prop MH 13A	Prop MH 14A	375mm – 100m @ 0.22%	New pipe
Notion Road	Prop MH 14A	SAN MH 35-29	375mm – 102m @ 0.22%	New pipe
Notion Road	Prop MH 35-29	Prop MH 35-30	450mm – 72m @ 0.22%	Replacement pipe
Notion Road	Prop MH 35-30	Prop MH 17	450mm – 4m @ 0.23%	Replacement pipe

Table 2 – Offsite sewer improvements

Note: Notion Road pipes are temporary and will be replaced by the Ultimate Regional Trunk sewer that will be directed South on Notion Road to the downstream SP.

#### 4. WATER SUPPLY AND DISTRIBUTION

#### EXISTING SYSTEM:

First Pickering Place (FPP) existing water service is fed from a 300 mm Ø City main on Pickering Parkway. The Plaza has a 300mm Ø service main off of Pickering Parkway with a series of hydrants and lateral services inside the Plaza to feed the multiple buildings. Refer to Exhibit 7 for the Regions existing water system.

#### **REDEVELOPED SITE:**

#### **Fire Protection**

Fire flows for Phase 1 will be supplied by a 300mm PVC fire service proposed to connect to the 300mm watermain on Pickering Parkway at two locations to provide a looped system complete with an isolation valve on the Pickering Parkway mainline. The proposed looped system will surround the existing single storey brick retail building, refer to Figure 3 in Appendix E for details on layout of the proposed Phase 1 looped watermain system.

As per Ontario Building Code 3.2.9.7 (4), Residential Towers being over 84m tall require an additional source of water supply from a public water system. To meet this requirement a second 300mm PVC fire service will be connected to the looped 300mm watermain with isolation valves installed on the 300mm watermain between the two fire services. Isolation valves will also be installed at Pickering Parkway to create redundancy in the system.

Refer to Figure 3 in Appendix E for details and locations of proposed watermain services.

#### **Domestic Water Service**

The domestic water supply is proposed to connect to the existing 300mm watermain on Pickering Parkway with a proposed 300mm PVC watermain. Refer to Figure 3 in Appendix E for location of proposed water services.

#### **Proposed Site**

The pressures and volumes must be sufficient for Peak hour conditions and under fire conditions as established by the Ontario Building Code. The MOE minimal residual pressure under fire conditions is 140 kPa (20.3 psi). According to the Durham Region, Design Criteria for Water mains the allowable pressures are as per Table 3.

SCENERIO	DURHAM REGION CRITERIA Allowable Pressure (kPa)		MOE Allowable Pressure (kPa)		
	min max		max	max	
Min. Hour	275	700	275	700	
Average Day	275	700	275	700	
Max Day	275	700	275	700	
Max Hour	275	700	275	700	
Maximum Day + Fire	140	700	140	700	

Table 3 – Allowable pressures

In order to evaluate the potential water demand for fire protection, the development was assessed using the Fire Underwriters Survey (FUS) guide. As shown in Appendix C, the following assumptions were made to perform the calculations;

1. Proposed buildings shall be of Fire Resistive type construction, therefore a construction type coefficient of 0.6 will be applied.

Proposed buildings shall be equipped with an automatic sprinkler system which meets NFPA 13 sprinkler standard including a fully supervised system, system to be designed by Mechanical Engineer.

The water demand requirement for the site based on the new population is calculated as follows:

Resid	ential (Domestic)		
a)	Average Day domestic demand -	using 364 L/cap/day (1575 persons)	6.64 L/s
b)	Max day demand -	1.9 x daily demand	12.61 L/s
c)	Peak hour demand -	2.85 x daily demand	18.91 L/s
Comn	nercial (Domestic)		
a)	Average Day domestic demand -	using 5000 L/m²/day (1687.6m²)	0.10 L/s
b)	Max day demand -	1.9 x daily demand	0.19 L/s
c)	Peak hour demand -	2.85 x daily demand	0.53 L/s
d)	Fire flow		167 L/s

Flow testing was conducted and results analysed using a hydraulic model KYPIPE for the full development site in the MSS report by Odan Detech. Available flow results from the report are shown below.

Table 4 – Total Water Demand For Phase 1 – First Pickering Place						
L/s USGM						
Peak Day Demand	12.79	203				
Fire Flow Demand	166.67	2,642				
Total Water Demand	2,748					
Available Flow at Block 1 (from MSS) 234 3,579						

The total water demand for the Phase 1 development is 179.5 L/s which is less than the available flow of 234 L/s. Therefore, the existing flow within the system is adequate to meet the domestic and fire demands for the proposed Phase 1 site.

#### FIRST PICKERING PLACE FUNCTIONAL SERVICING AND STORM WATER MANAGEMENT REPORT PICKERING, ONTARIO



Exhibit 7 Durham Region layout of existing water system

#### DISCUSSION OF RESULTS:

- The pipe sizes shown are required for the fire flows and to ensure velocities are below 5.0 m/sec for fire flows.
- First Pickering Place will require new mains and hydrants. Some will be relocated to suit the development.
- The pipe sizes chosen are adequate.
- Where pressures are greater than 80 psi (550 kPa) buildings will require pressure reducing valves prior to meter connection. Hydrant tests prior to permit stage will confirm this.
- Looping the watermain connection to Pickering Parkway is required to provide redundancy in the system for the development since buildings are taller than 84 m. The OBC requires a second connection to a public system when buildings are greater than 84 m.
- Phase 1 requires an interim condition watermain which will be looped around the existing retail building to provide a redundancy to the system. For layout and details of the proposed Phase 1 watermain looped system refer to Figure 3 in Appendix E.

#### 5. STORMWATER MANAGEMENT & FOUNDATION WATERPROOFING

#### Design Criteria

Stormwater management for the proposed development will follow the stormwater management criteria set out by the City of Pickering, Toronto and Region Conservation Authority and the Ontario Ministry of the Environment, Conservation and Parks.

A summary of the stormwater management criteria applicable to the site are as follows:

#### **Quantity Control:**

Stormwater Management Criteria, prepared by TRCA, 2012. The TRCA criteria for Duffin's Creek are to control post-development peak flows to pre-development levels for all storms up to and including the 100-year storm (i.e., 2-, 5-, 10-, 25-, 50-, and 100-year storms) **except** for the main branches of the East and West Duffin's Creek where no quantity control is required. The subject site is located within the watershed designated by the TRCA as not requiring quantity control.

At the Pre-consultation for 1755 & 1805 Pickering Parkway the City of Pickering Storm water management criteria was outlined as follows:

Stormwater Management Criteria that must be included in the FSSR are as follows:

- Control of post-development peak flow rates to pre-development levels.
- A maximum runoff coefficient of 0.5 should be used to represent pre-development conditions.
- Follow Stormwater Management Design Guidelines, prepared by City of Pickering. Runoff Conveyance will be as follows, the minor system is to be designed to accommodate the 5-year storm, while the major overland system is to be designed for the 100-year storm event. Where there is no suitable overland flow route, the minor system must convey the 100-year storm after on site attenuation.

#### Existing Storm Servicing and Drainage Patterns

As-constructed and design plans and profiles drawings obtained from the Region of Durham and the City of Pickering show that the following storm sewers are located within and around the site.

Refer to Exhibit 8 for the existing storm sewer system and outlet for the Phase 1 subject site.

#### FIRST PICKERING PLACE FUNCTIONAL SERVICING AND STORM WATER MANAGEMENT REPORT PICKERING, ONTARIO





#### Exhibit 8 - City layout of existing Storm sewers and Site sewers

The drainage from the subject site can be summarized as follow:

- MTO box culvert discharges flow from Hwy # 401 to a short ditch on the south side of the subject site. The flow is captured by an inlet structure attached to an existing 1200 ø storm sewer system which is routed north to Pickering Parkway where it discharges to a 1200 ø existing storm on Pickering Parkway. The pipe continues east on Pickering parkway, changes pipe sizes as shown on Exhibit 8, crosses Notion Road, continues east and discharges via a head wall to a drainage channel which empties into Duffin's Creek.
- 2. The subject site drains via a series of catch basins and sewers which connect to the 1200 ø storm from the 401 to Pickering Parkway as described in 1 above.
- The overland flow from the site is conveyed more or less from the south through the lands onto the Pickering Parkway and ultimately conveyed via Pipes and existing channel, east of the Notion Road, to the Duffin's Creek.
- 4. Currently, there is no stormwater quantity, quality control measures implemented within the existing site.

A pre-development tributary plan has been prepared based on a drainage pattern analysis of the site's digital terrain model created from existing topographic survey and information obtained from the Region and the City. The pre-development storm tributary plan is included in Appendix E.

#### **Pre-development/Allowable Flow Rates**

The post-development flows from the site will be limited to the pre-development flows for the 2-year to 100-year design storm event. The pre-development flows were calculated based on pre-development tributary area of **0.92 ha** with runoff coefficient of 0.5. Please note that the actual runoff coefficient for the existing site condition is much higher than 0.5. The predevelopment condition consists mainly of asphalt paved parking areas and rooftop.

The flows were calculated using both rational method and hydrologic model. The City of Pickering's Intensity Duration Frequency (IDF) curve values were used for rational method calculation.

The hydrodynamic model (XPSWMM) was used to simulate flows for pre-development condition. The Atmospheric Environment Service (AES) 1-hour and 12-hour storm hyetographs and the Chicago 4-hour storms provided in the City of Pickering's SWM design guidelines were used for pre-development condition peak flow simulation. For modeling the site under existing condition, the calculation of effective rainfall in XPSWMM was accomplished using the EPA runoff method. Losses are calculated using the Horton infiltration method and initial abstraction of 1 mm and 5 mm for impervious and pervious areas respectively.

The allowable flows for the site are presented in Table 6.

- The City 2 to100 year Chicago 4 hour, AES 1-hour and 12-hour Storms were used.
- Horton infiltration parameters were used for soil types C.

 $F_0 = 75$  mm/hr,  $F_c = 5$  mm/hr, decay rate  $\dot{\alpha} = 0.000556$  1/sec

• Flows were calculated using the EPA SWMM5 runoff method (similar to Stanhyd in VO2).

• Area = 0.92 ha, w= 58.7 m, C=  $0.5 \rightarrow \%$  impervious = 43%

 $TIMP = (C - 0.2) \div 0.7 = 0.43$ 

- TIMP = total impervious fraction (dimensionless)
- C = runoff coefficient

Table 5 – Comparison Existing flows to Phase 1 – Out pipe at EX.MHS3							
			Storm	п Туре			
Storm Event	Existing Conditions Phase 1 Conditions						
	Chicago 4 hr (m3/s)	AES 1 hour (m3/s)	AES 12 hour (m3/s)	Chicago 4 hr (m3/s)	AES 1 hour (m3/s)	AES 12 hour (m3/s)	
2- year	1.975	1.572	0.558	1.872	1.452	0.561	
5- year	2.779	2.341	0.724	2.637	2.180	0.729	
10- year	3.327	2.854	0.837	3.145	2.668	0.843	
25- year	3.988	3.541	1.006	3.796	3.322	1.010	
50- year	4.475	4.042	1.118	4.259	3.801	1.122	
100- year	4.891	4.454	1.227	4.753	4.216	1.231	

Table 6 shows the flows from the site only. The flows shown in table 5 is flow from the MTO culvert and the site.

Table 6 – Targ	Table 6 – Target Peak Flows from Phase 1 site ( <b>allowable</b> )												
Storm Event	Chicago 4 hr (m3/s)	AES 1 hour (m3/s)	AES 12 hour (m3/s)	Rational method for comparison using IDF curves									
2- year	0.110	0.084	0.036	0.079									
5- year	0.189	0.148	0.053	0.108									
10- year	0.244	0.196	0.063	0.128									
25- year	0.312	0.258	0.076	0.168									
50- year	0.360	0.305	0.085	0.205									
100- year	0.401	0.349	0.094	0.237									

Rational method uses As per City criteria for; 25-year storm - Ca = 1.10 50-year storm - Ca = 1.20 100-year storm - Ca = 1.25 C = 0.5 for 2 to10 year events, Tc = 15 min (conservative)

Rational method is very similar to EPA runoff using the City IDF curves (Chicago storms).

The City of Pickering uses the AES storm for sizing SWMM facilities.

#### **POST-DEVELOPMENT**

The SWM for the redeveloped First Pickering Place will establish/analyse the following:

- 1. Flows to the existing 1200 ø storm sewer based on the criteria established above.
- 2. Establish SWM criteria for Phase 1 in order to limit the flows.
- 3. Evaluate the flows entering the down-stream sewer system at the outlet.
- 4. Evaluate the water quality requirements.
- 5. Evaluate the water balance for the Site.
- 6. Make recommendations as to the implementation of the SWM.

#### Hydrology and Hydraulics:

We will utilize a Hydrodynamic model to evaluate the sewer items such as flow, velocity, HGL along with the above-mentioned items. The Hydrodynamic model we will use is XPSWMM by INNOVYZE version 2021. XPSWMM is using the modified EPA SWMM 5 engine. SWMM 5 models can be imported and exported into XPSWMM. The Hydrodynamic models provide the most accurate, reliable and defensible representation of flows in the collection system. They account for varying inflows, non-coincident peak flows, in system storage, hydrograph attenuation, and tail and backwater effects. The hydrology will be done using the SWM runoff methods which is similar to Otthymo Standhyd. In addition, if rural watersheds are required, XPSWMM fully implements the Nash unit hydrograph technique. The peak flows for these small tributary areas can be hand verified using the rational equation. XPSWMM will balance the entire system such as stage/storage/discharge without having to input orifice type equations. The added feature of XPSWMM is the integrated 1D/2D capability.

#### What to Model:

Based on the description of the existing system, and the imposition by the City of flow reduction to a C =0.5 from the existing site C= 0.85 (See table 6 above). The post developed site will reduce flows to the outlet at the existing 1200  $\emptyset$  sewer. Phase 1 allows outlet to the existing 1200  $\emptyset$  sewer. Refer to Appendix E for the site servicing drawings.

Therefore, the model will include the flow from the MTO culvert and the new site sewers. The boundary conditions are outfall at the existing EX.MHS3.

The City of Pickering uses the AES storm for sizing SWM facilities. It will be shown that the 4 hour Chicago storm is the critical storm for all storage facilities.



24

#### Exhibit 10- XPSWMM PHASE 1 MODEL WITH TRIBUTARY AREAS



#### Exhibit 11- XPSWMM profile plot STM TANK to EXMH5 – 100-YR Chicago



	Still Barris	BEOCKT	111111	1411-15	141112	141110-1	EXITY 100	EXTENSION OF	EXTENSION 101	EX WITE
Storm	100yr4hrChicago									
Ground Elevati	90.500	90.471	88.934	88.853	87.952	86.330	86.667	85.690	84.888	84.851
Max Water Ele	87.959	86.608	86.288	86.087	85.546	85.295	85.248	82.937	81.848	81.496
Max Water De	1.573	0.225	0.243	0.317	0.416	1.305	3.358	1.857	1.208	1.139
Invert Elevatio	86.386	86.386	86.045	85.770	85.130	83.990	81.890	81.080	80.640	80.357
Max Volume	235.943	0.274	0.296	0.387	0.508	1.606	4.101	2.269	1.474	1.390

26

#### Exhibit 12- XPSWMM profile plot STM TANK to EXMH5 – 5-YR Chicago



NODE budmlogu

#### **XPSWMM MODEL:**

The XPSWMM model is a series of node Links forming a 1D dynamic model with hydrology and hydraulics coupled together. Flow (runoff) is calculated at nodes and dynamically routed through pipes, culverts, storage structures and open channels. The following are the info used in the model:

- All plastic and concrete pipes Manning n = 0.013.
- All CSP pipes Manning n = 0.024.
- All open channels Manning n = 0.040 (considering dense vegetation along the channels).
- Pipe Manhole loss coefficients for entrance and exit were accounted for via drop in manhole inverts.
- Pipe obverts were more or less matched.
- XPSWMM was chosen to accurately show the HGL.
- Refer to sewer profile plots for calculations of flows and other hydraulic stats.
- XPSWMM in 1D, uses a Finite difference Runge-Kutta explicit scheme. Scheme solves all terms of the St.Venant equations. 1D and 2D schemes automatically switch between upstream and downstream controlled flow regimes to represent shocks.

#### TIME STEP:

to 1.25 sec or less.

We have adapted the following time steps: 1D model start with 15.0 sec. Note the explicit nature of the algorithm automatically reduces the time step. In the case of this model the program has reduced the time step

- The City 2 to 100 year 4-hour Chicago, AES 1-hr and AES 12-hr Storms were used.
- Horton infiltration parameters were used for soil types C and D.

 $F_0 = 75 \text{ mm/hr},$   $F_c = 5 \text{ mm/hr},$  decay rate  $\dot{\alpha} = 0.000556 \text{ 1/sec}$ 

Depression storage 1mm impervious and 5mm pervious

Refer to table 7 for the existing XPSWMM model hydrology parameters. Refer to Exhibit 9 for the Proposed Site XPSWMM model.

			Impervious				Infiltration	Time to Peak
Name	Subcatchment	Area ha	Percentage %	Width m	Slope m/m	Hydrology Methods	Reference	Tp (min)
EX.MHS6		0	0	0	0	SWMM Methods 64		0
EX.MHS3	1	0.282	99	32.5	0.01	SWMM Methods 64	ROOF	0
EX.MHS3	2	0.57	99	62.2	0.01	SWMM Methods 64	ROOF	0
EX.MHS3	3	0.921	99	58.8	0.01	SWMM Methods 64	ROOF	0
EX.MHS3	4	0.606	88	47.7	0.016	SWMM Methods 64	Parking	0
EX.MHS3	5	0.341	95	35.8	0.012	SWMM Methods 64	Parking	0
EX.MHS2		0	0	0	0	SWMM Methods 64		0
EX.MHS1		0	0	0	0	SWMM Methods 64		0
EX MH5		0	0	0	0	SWMM Methods 64		0
EX.CHMHS9	1	0.15	99	23.7	0.046	SWMM Methods 64	Parking	0
EX.CHMHS9	2	0.058	99	14.7	0.011	SWMM Methods 64	Parking	0
EX.MHS8	1	0.258	80	31.1	0.02	SWMM Methods 64	Parking	0
EX.MHS4	1	1.347	91	69.2	0.034	SWMM Methods 64	Parking	0
EX.MHS4	2	0.271	68	31.9	0.005	SWMM Methods 64	Parking	0
EX.DCB4	1	0.593	90	47.2	0.013	SWMM Methods 64	Parking	0
EX.DCBMHS7	1	0.975	90	60.5	0.027	SWMM Methods 64	Parking	0
EX.DCB9	1	0.29	97	33	0.007	SWMM Methods 64	Parking	0
MTO culvert	1	41.635	10	395.1	0.009	SWMM Methods 64	OFF SITE	0
MH1	1	0.235	85	29.7	0.02	SWMM Methods 64	Urban-C-soils	0
MH2	1	0.16	85	10	0.01	SWMM Methods 64	Urban-C-soils	0
MH3	1	0.123	85	21.5	0.01	SWMM Methods 64	Urban-C-soils	0
MH3	2	0.1	15	19.4	0.01	SWMM Methods 64	Urban-C-soils	0
MH5		0	0	0	0	SWMM Methods 64		0
MH6-1		0	0	0	0	SWMM Methods 64		0
<b>STM TANK</b>	1	0.92	85	58.7	0.01	SWMM Methods 64	ROOF	0
BLOCK 1		0	0	0	0	SWMM Methods 64		0
MH4		0.92	85	0.587	0.01	SWMM Methods 64		0

#### Table 7 – Proposed XPSWMM model hydrology parameters

#### DISCUSSION OF XPSWMM MODEL:

- 1) The Model tributary areas follow the minor system tributary areas. See model above.
- 2) There are no celerity issues with the model. There were no warnings or errors.
- 3) All conduits were stable. The continuity error was less than 1% in all storm runs which is considered excellent.
- 4) There were no warnings or error messages from the analysis.
- 5) In a dynamic model the orifice size and co-efficient are entered. The Model calculates the HGL and volume required. There is no need for a rating curve.
- 6) Outfalls are considered free flow, since the outlet is to a trunk sewer.
- 7) The HGL plots show the brown service line as the spill crest when representing surface storage nodes and rim elevation for MH nodes. The plots are for the 5 year and 100-year storms.
- 8) The long plots (profile) have tables that give hydraulic stats for each length of run.
- 9) The stats show that the City criteria for sewers has been achieved.

#### Phase 1 Analysis Results

Table 8 – Peak Flows from Phase 1 Site												
Storm Event	Р	Allowable eak Flow (m3	3/s)	Phase 1 Peak Flow (m3/s)								
	Chicago 4 hr (m3/s)	AES 1 hour (m3/s)	AES 12 hour (m3/s)	Chicago 4 hr (m3/s)	AES 1 hour (m3/s)	AES 12 hour (m3/s)						
2 year	0.110	0.084	0.036	0.074	0.068	0.043						
5 year	0.189	0.148	0.053	0.103	0.096	0.057						
10 year	0.244	0.196	0.063	0.120	0.113	0.066						
25 year	0.312	0.258	0.076	0.138	0.132	0.077						
50 year	0.360	0.305	0.085	0.150	0.145	0.086						
100 year	0.401	0.349	0.094	0.163	0.157	0.094						

Phase 1 Site Flow is site out-pipe flow at MH4.

## Note the post development flows to the City sewer is reduced considerably due to storage tanks.

#### SUMMARY OF SWM Quantity Control Features:

Refer to Table 9 for the SWM used for quantity control of Phase 1.

#### Table 9 – SWMM Quantity Features for Phase 1

BLOCK OR DESCRIPTION AND FLOW AREA TO TANK (ha)	SWMM FEATURE DESCRIPTION & FOOTPRINT (m2)	VOLUME REQUIRED 100-year flow (m3) max of 4 hr Chicago or AES	ORIFICE CONTROL C=0.62	ORIFICE max head (m)	Maximum 100-year flow (L/sec)
BLOCK 1 (0.919 ha)	1-Storage Tank (150)	TANK 1 – 236	250 mm	1.57	163

Maximum Volume created by 4-hour Chicago storm

#### FOUNDATION WATERPROOFING STRATEGY

Dewatering discharge during construction and long term will be as follows:

At the Pre-consultation for 1755 & 1805 Pickering Parkway the City of Pickering made the following statement:

## Please note that the City will not accept discharge of foundation drainage to the storm system due to the potential for adverse impacts.

## Please note that Region of Durham will not accept discharge of foundation drainage to the sanitary sewers. This statement is part of their sewer bylaw.

Based on the above we recommend the Architect, Structural Engineer, Geotechnical Engineer and Mechanical Engineer devise a waterproofing system with the shoring and foundation design.

Based on the above we have not incorporated any allowance for foundation drainage in the SWM for the site.

#### DISCUSSION OF RESULTS:

- The outlet for Phase 1 can be the existing 1200mm dia. storm sewer since the Phase 1 quantity controls will reduce the flow entering this pipe
- Phase 1 requires 236m<sup>3</sup> of storage for quantity control to meet the City of Pickering SWM design guidelines, storage volume will be provided by means of a storm water management tank located in the underground parking levels
- Orifice control for the storm water management tank will be a 250mm dia. orifice plate
- Flows from the site will be reduced at Phase 1 of the development, further flow reduction will occur at each subsequent phase of the ultimate build out (See MSS report by Odan Detech for further details)

#### 6. WATER BALANCE

The primary objective of the Water Balance Targets/Criteria is to capture and manage annual rainfall on the development site itself to preserve the pre-development hydrology (or "water balance", which typically consists of three components: runoff, infiltration, and evapotranspiration) through a combination of infiltration, evapotranspiration, landscaping, rainwater reuse and/or other low impact development practices.

#### Site Criteria

In most cases, the minimum on-site runoff retention requires the proponent to retain all runoff from a small design rainfall event – typically 5mm through infiltration, evapotranspiration and rainwater reuse.

The City of Pickering Stormwater Management Design Guidelines' target for water balance is to provide runoff reduction from the site through infiltration, evapotranspiration and reuse of a minimum of 5mm of rainfall depth across all impervious surfaces.

#### CITY OF PICKERING GUIDELINE WATER BALANCE SUMMARY

#### Project: 1755&1805 Pickering Parkway (First Pickering Place) Project No.: 20266

		_
Site Area	7825	]m <sup>2</sup>
Rainfall depth required to capture	5	mm
Captured Volume Target (5mm across entire s	39.1	m <sup>3</sup>
(Total Area x Rainfall Depth)		

SURFACE TYPE	SURFACE CAPTURE (mm)	AREA (m²)	% OF SITE AREA	VOLUME CAPTURE (m³)
Green Roof	7	682	8.7	4.8
Landscaped Areas	5	921	11.8	4.6
Roof Area (Drains to Cistern for Reuse)	12.86	2309	29.5	29.7
Asphalt Driveway, Pavers and Concrete (Ground)	0	3913	50.0	0.0
TOTAL		7825	100	39.1

#### CAPTURED VOLUME BY INTIAL ABSTRACTION (m<sup>3</sup>) 9.4 VOLUME OF CISTERN (m<sup>3</sup>) 29.7 CAPTURED VOLUME (m<sup>3</sup>) 39.1

The site area and 5mm rainfall depth will be used to calculate the water balance target. The water balance target is as follows.

Water Balance Target:

Site Area\* x 5mm = (7825m<sup>2</sup> x 0.005m) = 39.1m<sup>3</sup> \*Site area does not include 14m MTO Setback Lands.

It is proposed to achieve the above target through infiltration/absorption and rainwater harvesting for reuse.

The water balance summary that follows, summarizes the rain capture over the site. The site was divided according to surface conditions, and an initial abstraction value (IA) or the expected capture depth was derived for each surface condition. **9.4m<sup>3</sup>** will be captured by initial abstraction.

Therefore, in order to achieve the required water balance target, rain harvesting of storm run-off from the roof top to a cistern will be implemented, with a potential volume of **29.7m**<sup>3</sup>. This volume can be used for irrigation of landscaping, greywater toilets in the retail spaces and greywater wash-down areas in the underground parking levels. Detailed calculations for water reuse consumption is located in Appendix D. The stormwater retention/water balance tank can be located within the SWM tank as chambers or individual tanks.

Further detail on water reuse will be presented in the Stormwater Management Report at the Site Plan Approval stage. Preliminary calculations are shown below.

Water Balance Summary:									
Water Balance Target:	39.1m³								
<u>Capture:</u>									
Initial Abstraction (Absorption/ Infiltration/ Evapotranspiration)									
Green Roofs Planters & Landscaping	4.8m³ <u>4.6m³</u>								
Total Captured Volume by Initial Abstraction	9.4m³								
Capture in Cistern from Roof Top for Reuse	<u>29.7m³</u>								
Total Volume Capture	39.1m <sup>3</sup>								
Reuse Potential from Cistern									
Greywater toilet and urinal reuse (Retail) Irrigation requirement for landscaping Greywater wash-down area reuse (Underground Parking)	TBD TBD TBD								
Total Reuse Potential from Cistern	>29.7m <sup>3</sup>								
The total capture of 39.1m <sup>3</sup> meets the target volume of 39.1m <sup>3</sup> ; therefore, the water balanced target can be achieved on site. In addition, the total on-site water re-use									

potential of shall exceed the minimum cistern capture requirement of 29.7 m<sup>3</sup>.

#### 7. WATER QUALITY

The water quality target for the subject development as required by City of Pickering is Enhanced Level of Protection - long term average removal of 80% Total Suspended Solids (TSS) on an annual loading basis from all runoff leaving the proposed development site based on the post-development level of imperviousness.

The site was divided according to surface conditions and the effective TSS removal for each surface condition was considered based on the treatment it would receive. The general basis of the effective TSS removal rates are as follows:

1. Rooftop areas are subject only to airborne particles and insignificant amounts of sediment transported by foot traffic. As such, an effective removal efficiency of 80% is utilized on a conventional roof to reflect the inherent runoff quality from a conventional roof.

2. Balconies and sodded areas are subject to insignificant amounts of sediment transport by foot traffic. An effective removal rate of 80% is used.

3. Driving and ground-level pedestrian surfaces which are open-to-above will be subject to Winter maintenance, therefore they are assumed to have an effective removal efficiency of 0% and filtration is thus required.

Block 1 is comprised of open-to-above driving and pedestrian areas which will be subject to future winter maintenance. Oil and Grit Separation (OGS) devices will be specified accordingly to provide 80% TSS Removal for the site. Flows from asphalt driveway, paver and concrete areas will be directed to an Oil/Grit Separator sized accordingly for the development prior to entering the SWM Tank.

Through the above inherent TSS removal rates and the OGS unit, the 80% TSS removal rate can be achieved.

#### 8. GRADING CONSIDERATIONS

The existing topography of the site generally slopes from west to northeast towards the low point of the site located on the east side of the Site. Under the new development and existing adjacent developments there are several grading constraints for this development to match. The constraints are the existing commercial buildings, intersection at Brock Road and MTO lands to the south.

For proposed grading of the redeveloped site refer to the Preliminary Grading Plan included in Appendix E.

#### 9. EROSION AND SEDIMENT CONTROL

Erosion and sediment controls for the site will be implemented according to the Golden Horseshoe Area Conservation Authorities' Erosion and Sediment Control Guidelines for Urban Construction. A detailed erosion control plan will be prepared upon final design and at Site Plan Approval Stage.

#### 10. SOILS REPORT AND HYDROGEOLOGY:

A preliminary Geotechnical investigation has been completed for the site. The purpose of the study is to characterize hydrogeological conditions and determine permitting requirements for the proposed development at the First Pickering Place. The study was completed by Terraprobe dated May 27, 2021 for Pickering Ridge Lands Inc. & Bayfield Realty Advisors.

Native clayey silt glacial till, underlying dense to very dense matrix of sandy silt to silty sand till is the typical soil underlying the site. The soils have some infiltration capacity. The water table underneath varies from 4 to 6 m below grade. Based on the grading it may be possible to provide infiltration galleries. The water table should be monitored further in order to get a wide range of potential water table levels. Monitoring will provide better confidence in the potential maximum ground water levels.

#### 11. **RECOMMENDATIONS**:

- We recommend that the owners of First Pickering Place build the sanitary sewer on Pickering Parkway from 1899 Brock Road site to Notion Road to accommodate the full build out of all future development sites and the existing flows. This section of sanitary sewer will be subject to development charges as discussed with the Region of Durham.
- 2) The sanitary pipe on Notion Road (from Pickering Parkway to Orchard Rd) will be sized to convey existing flows and flows from Phase 1 (First Pickering Place) to the existing Orchard Road sanitary sewer. The Region will allow this interim condition at limited capacity until such time that the Ultimate Trunk Sewer is constructed in the future to convey flows to the South SP. The interim pipe will be downsized from that on Pickering Parkway, the Region will allow this, since it is a temporary measure until the Region replaces it with a trunk sewer on Notion Road.
- 3) We recommend looping the watermain to Notion Road or Brock Road to provide redundancy to the development since many buildings are taller than 84 m. The OBC requires a second connection to a public system when buildings are greater than 84 m.

#### 12. CONCLUSIONS

The findings of our investigation and analysis can be concluded as follows:

The proposed site is serviceable with the added density with respect to sanitary, water and storm by connecting to the existing infrastructure in and around the site as outlined in this report.

Table 10 – Summary Information for	Proposed Re-Development
Allowable release rate from site (L/s)	401 L/s
Actual release rate from site (L/s) (100-year storm)	163 L/s
Total Stormwater Storage Volume Required/Available in U/G Parking SWM Tank	236 m <sup>3</sup>
Cistern Tank For Stormwater Reuse	29.7 m <sup>3</sup>
Orifice tube size used	250 mm
Water Quality	80% TSS achieved by nature of proposed development (i.e. all roof top & amenity) with OGS unit for driveways, pavers, and concrete

Table 10 summarizes the SWM components of the proposed development.

#### 13. REFERENCES

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- 3. TRCA (August 2012). **Stormwater Management Criteria**, Version 1.0. Toronto and Region Conservation Authority, Ontario.
- 4. GGHA CAs (December, 2006). **Erosion and Sediment Control Guideline for Urban Construction**, Greater Golden Horseshoe Area Conservation Authorities, Ontario.
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- 6. Ontario Ministry of the Environment (2008). **Design Guidelines for Drinking-Water Systems**. Ministry of Environment, Ontario. ISBN 978-1-4249-8517-3.
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- 11. FEMA Chapter 4 Flood Risk Assessment.
- 12. ROAD AND BRIDGE DECK DRAINAGE SYSTEMS by MTO, November 1982.
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- 15. LOW IMPACT DEVELOPMENT STORMWATER MANAGEMENT MANUAL, 2008, by Credit Valley Conservation Authority and Toronto Town Conservation Authority.
- 16. **Master Servicing and Stormwater Management Report**, for 1899 Brock Road, City of Pickering, May 2021 by SCHAEFFERS.
- 17. Functional Servicing & Stormwater Management Report Residential Townhouse Development – 1856 Notion Road Durham Region – City of Pickering, January 19, 2018, by GHD.
- City of Pickering and Pickering Developments Inc. New Highway 401 Road Crossing (from Notion Road to Squires Beach Road) Schedule "C' Municipal Class Environmental Assessment, October 2019, by AECOM.
- 19. **Master Servicing and Stormwater Management Report**, 1755 & 1805 Pickering Parkway, City of Pickering, January 2022, by ODAN/DETECH Group.

Respectfully Submitted: The Odan Detech Group Inc.

Date: April 20, 2022



John Krpan, M.S.C.E., P.Eng.

Scott Ahonen, B.Eng.

#### **APPENDIX A**

Aerial Photo of Existing Site Phase 1 Site Plan of the Proposed Development (reduced) Ultimate Site Plan of the Proposed Development (reduced)

#### Aerial Photo of Existing Site





#### Phase 1 Site Plan of the Proposed Development (reduced)



#### Ultimate Site Plan of the Proposed Development (reduced)

FILE No. 20266 - Bayfield-1755&1805 Pickering Pkway - FSR Phase 1 - APR 2022

#### **APPENDIX B**

Redeveloped site Phase 1 sanitary sewer design sheet

Redeveloped sites (subject site, 1899 Brock Road and surrounding tributaries) sanitary sewer design sheet

#### Redeveloped subject site Phase 1 sanitary sewer design sheet

													DESIGNE		0000			022 04 0	6					
SCENARIO 2:	PHAS		15										DESIGNE	DB1.3.AI				022-04-01	0					
OOEIIANO E.	Redev	eloped subject s	site Phase 1 s	anitar	y sewer o	design sh	eet PROPOSE	D PIPE	<b>E SIZES</b>				CHECKE	DBY:M.AF/	\w ad									
												· · ·							_				PRESENT	
							RESIDENTIAL				ERCIAL				FLOW (I	⊔s)			E	XISTING	SEVVER		CONDITION	
		UPSTREAM	DOWNSTREAM		TARFA	POP	POP # OF	POP	PEAK	тот	FLOOR	GROS	S ELOOR	RESIDEN		COMM	TOTAL				Full Flow			1
STREET	TRIBID	мн	мн			DENSITY		3	FLOW		SPACE	Δ	RFA			2.08	FLOW	Length	Size	Slope	Canacity	Velocity	% Full	NOTES
					ACCUM	/Porsons/	(Persons		FACTOR	(Ha)		GEA			SBMACE	Ve	Ve		n	6	Ocan	V	-	
				(he)	(ha)		(10130113					(ha)	(ba)	0.26 (1./2)	0.0042 (1./2)				(		(1.4-)	(	0(4)/0	-
				(IIA)	(11a)	114)	701m)	_	<u>г</u> н			(IIA)	(IIa)	0.20 (03)	0.0042 (115)			(11)	(nn)	(70)	(US)	(115)	Q(0)/Qcap	
Canadian Tire Site	4	EX.MH090	EX MH 34-82									0.79	0.79	9		1.65	1.65	59.8	200	0.30	17.96	6 0.57	9.2	
Pickering Parkw ay		EX MH 34-82	Prop MH9A	0.52	0.52	2							0.79	0.14	0.00	1.65	1.78	49.4	675	0.37	511.31	1.43	0.3	pipe sized for full build-out
Subject Site	P1	Prop MH1A	Prop MH2A	1.18	1.18	8	2.5 63	0 1575	5 3.6 <del>6</del>	5		0.17	0.17	7 0.31	24.24	0.35	24.90	20.7	300	0.87	90.20	0 1.28	27.6	pipe sized for full build-out
Subject Site		Prop MH2A	Prop MH3A		1.18	3		1575	5 3.66	5			0.17	7 0.31	24.24	0.35	24.90	44.7	300	0.95	94.25	5 1.33	26.4	pipe sized for full build-out
Subject Site	P2	Prop MH3A	Prop MH4A		1.18	3		1575	5 3.66	;		0.28	0.45	<b>5</b> 0.31	24.24	0.93	25.48	83.5	300	0.78	85.40	0 1.21	29.8	pipe sized for full build-out
Subject Site		Prop MH4A	Prop MH1A-1		1.18	3		1575	5 3.66	6			0.45	0.31	24.24	0.93	25.48	97.4	300	0.55	71.72	2 1.01	35.5	Interim pipe Phase 1
Subject Site	P3,2	Prop MH1A-1	Prop MH7A		1.18	3		1575	j 3.66	5		1.50	1.95	0.31	24.24	4.05	28.60	45.4	300	0.31	53.84	0.76	53.1	Interim pipe Phase 1
Subject Site		Prop MH7A	Prop MH8A		1.18	3		1575	5 3.66	;			1.95	5 0.31	24.24	4.05	28.60	29.9	450	0.52	205.59	1.29	13.9	pipe sized for full build-out
Subject Site		Prop MH8A	Prop MH9A		1.18	3		1575	5 3.66	5			1.95	0.31	24.24	4.05	28.60	14.3	450	0.72	241.92	2 1.52	11.8	pipe sized for full build-out
		•	·																					1
Pickering Parkway		Prop MH9A	EX MH 34-83	0.25	1 95	5		1575	36				274	0.51	24 24	5 70	30 44	42.0	675	0.33	482 88	1 35	63	pipe sized for full build-out
Pickering Parkway		FX MH 34-83	EX MH 35-5	0.24	2 19			1575	366				2.1	0.57	24.24	5.70	30.51	100.0	675	0.00	588.41	1.60	52	pipe sized for full build-out
Pickering Parkway	15	EX MH 35-5	EX MH 35-6	0.2	2.10	/		1575	3.66	,			2.7	10.0	24.24	5.70	30.58	00.0	675	0.48	582 38	1.01	53	pipe sized for full build-out
FICKETING FAIKWAY	1.5			0.20	2.47			15/5	J <u>J.</u>	' <u> </u>			2.1-	+ 0.04	24.24	5.70	30.30	35.0	0/3	0.40	302.30	1.03	J.J.J	
	-			2 00	2.00			479	2 2 0/	<u> </u>				0.75			3 53	50.0	200	0.05	21.07	1 00	11.0	
				2.08	2.05			173	5 3.00	'				0.75	2.11		3.52	59.0	200	0.95	31.97	1.02	11.0	
		D(1404		0.05		-		070							40.70		44.07			0.75				
METROHA	6	EX MH3A	EX MH 35-6	3.65	3.65	<u>'</u>		6/2	2 3.80	1				0.95	10.73		11.6/	38.2	200	0.75	28.40	0.90	41.1	
								_																
Pickering Parkway	16	EX MH 35-6	EX MH 35-7	0.22	9.23	8		2420	3.52	2			2.74	1 2.40	35.78	5.70	43.88	82.5	675	0.38	518.17	1.45	8.5	pipe sized for full build-out
Pickering Parkw ay	17	EX MH 35-7	EX MH 35-8	0.24	9.47	′		2420	3.52	2			2.74	4 2.46	35.78	5.70	43.94	80.0	675	0.46	570.11	1.59	7.7	pipe sized for full build-out
Pickering Parkw ay	18	EX MH 35-8	SAN MH 35-28	0.22	9.69			2420	) 3.52	2			2.74	4 2.52	35.78	5.70	44.00	110.1	675	0.57	634.63	8 1.77	6.9	pipe sized for full build-out
Subject Site	5	EX MH 35-34	EX MH 35-33									0.42	0.42	2 0.00		0.88	0.88	145.7	150	1.00	15.23	3 0.86	5.8	
Notion Road	20	EX MH 35-33	SAN MH 35-28	0.50	0.50								0.42	2 0.13		0.88	1.01	109.4	200	1.82	44.25	5 1.41	2.3	
MARSHCOURT DR		EX MH 35-8	EX MH 35-25		0.00				0.00	)				0.00	0.00	0.00	0.00	<del>58.9</del>	250	0.41	38.08	3 0.78	0.0	pipe to remain as cleanout access
ASHFORD DR	8	EX.MH023	SAN MH 35-25	1.93	1.93	60		116	3.80					0.50	1.85		2.35	73.0	200	0.40	20.74	0.66	11.3	
MARSHCOURT DR	9	SAN MH 35-25	SAN MH 35-26	0.29	2.22	2 60		133	3.80					0.58	2.13	0.00	2.70	72.8	250	0.55	44.10	0.90	6.1	
MARSHCOURT DR	10	SAN MH 35-26	SAN MH 35-27	0.60	2.82	2 60		169	3.80					0.73	2.70	0.00	3.43	70.3	250	0.55	44.10	0.90	7.8	
																								-
MARSHCOURT DR	11, 12	EX MH 032	SAN MH 35-27	17.39	17.39	60		1043	3.79			0.67	0.67	4.52	16.60	1.39	22.52	40.5	250	0.27	30.90	0.63	72.9	
	1,																							
FASEMENT		SAN MH 35-27	SAN MH 35-29	0.00	20.21			1212	374				0.67	5 25	19.07	1 39	25 71	124.0	375	0.16	70 13	0.63	36.7	1
			0	0.00									0.01	0.20	10.01		20.11	121.0				0.00		4
Pickering Parkw av	-	SAN MH 35-28	Prop MH 134	0.01	10.20			2420	3 52	,			3 16	2 65	35 78	6 58	45 02	14.5	375	0.22	82.24	L 0.74	54.7	Interim pipe Phase 1
	+	Pron MH 12A		0.01	10.20			3004	. 3.32		+	+	2.10	2.00	53.70	6.50	-J.UZ	100.0	275	0.22	82.24	. 0.74	78.0	Interim nina Phasa 1
	+		SAN MU 25 20	0.20	10.40	<u></u>		3004	1 J.J4			+	2.10	2.72	51 07	6.50	6/ 10	100.0	275	0.22	82.24	0.74	78.0	Interim nine Phase 1
	+			0.23	10.70	<u>'</u>		3904	r J.34	<u> </u>		+	J. 10	<u>, 2.70</u>	J4.02	0.00	04.10	101.0	- 3/3	0.22	02.24	0.74	10.0	
		SANIMU 25 00		0.05	34.40			E447	/ 20/				3.07	0 40	E0 54	7.00	05.64	74.0	AE0	0.22	122 72	2 0.04	64.0	Interim nine Phase 1
NOTION ROAD		SAN MH 35-29	SAN MH 35-30	0.25	31.10	2		5117	3.24				3.03	0.10	69.54	7.90	05.01	/1.0	450	0.22	133.73	0.04	04.0	
NOTION ROAD		5AN MH 35-30	SAN MH17	0.25	31.41			511/	3.24	•			3.8:	8.17	69.54	7.98	85.68	4.0	450	0.23	136.73	5 0.86	62.7	
		SANMH 17	SANMH 18		31 / 1			-			-						85.68		750	Availab	l la canacity	/ at Orchard	Rd 750mm dia	see note below, about canacity
		GATTINIT IA	0/111/0/1110		01.41												00.00		700		ю сараску 150 I /е			See This below about capacity
Bastan Galianta T		M	10 · 0 · 7		0 1 0		NOTES								an aitu bu Land	lles				Total fla		tod boro do	oc not include	
Av erage daily per capita f	ie Regiona low = 364 l	/cap/day (Residential	am Design Specifica  }	ations to	r Sanitary Si	ewers	1) MINIMU	VELOCI	TY = 0.60 m/s					Population D	ensity by Land	USe				the evin		ted here do		
Av erage daily per capita f	low= 180,0	000 L/GFA hectares/d	ay (commercial&ind	lustrial)			2) MAXIMU	M VELOC	ITY = 3.65 m/s				-	Housing Type			Densit	x	_	ule exis	any sania	ary now s co	inveyed south	
I = Unit of peak extraneous	s flow whe	n foundation drains ar	e NOT connected to	o the sto	rm sewer =	0.26 L/s/Ha	- 3) INFILTR	ATION 0.2	16  l/s = 22.5  m3	Ha/DAY	/Eoundatia	e Desle	-	Single & Semi	Detached		3.5 P/	u		on Notic		rchard Rd.		
Q(p) = peak population flo Q(d) = peak design flow (l	wv(⊔/s)Q(l √s)	) – peak extraneous f	iow(L/S)				Connect	ions)	nz 1/5 - 45.0 m3	na/DAT	(r oundatio	n Draifi		Apartment-2B	im		3.0 P/	u						
PEAKING FACTOR (Ham	non; Resid	ential) M =1 + 14/(4+(I	P/1000*0.5))				4) COMME	RCIAL 2.0	18 I/s (local sew	ers) 1.04	Vs (trunk s	ewers)										_		
PEAK POPULATION FLO	W, Q (p) =	q*P*M / 86400 L / Se	KC.				5) EXISTIN	G CONDI	TION INCLUDE	SCOMM	TIED DEV	VELOPME	NT -	Housing Type			Densit	Y.	-					
PEAK EXTRANEOUS FLO	(d) = Q(p)	+ Q(i) L / Sec.					7) COMME	RCIAL FL	OOR SPACE IN	IDEX=509	6 UNLESS	3		Semi Detache	d & Duplex		100 pe	sons/ha						UDAN•DETECH
PIPE ROUGHGNESS, n =	= 0.013 For	Manning's Equation														-								CONSULTING ENGINEERS
			1							1														
							3	ASSU	MED 150 L/s	VAILA	BLE EXC	ESS FLO	WCAPA	CITY AT OR	HARD ROAD	) as per co	rrespond	ence w it	h Durhar	n Region				
	-	1		1					1	T		1		1	1	1	1		1			-		

FILE No. 20266 - Bayfield-1755&1805 Pickering Pkway - FSR Phase 1 - APR 2022

	CONC	EPTUAL FULL	BUILDOUT C	ONDI	TIONS									DESIGNE	DBY:S.Ahor	nen		DATE: 20	022-04-13	3					
SCENARIO 3:	Full de	velopment of s	ubject site and	d future	e tributar	y sanitar	y design	sheet						CHECKED	BY: M. ALAV	w ad									
						<u>у</u> F	RESIDENTIA	L			COMME	RCIAL				FLOW (L	/s)			EX	ISTING S	SEWER	<u> </u>	PRESENT	
													00000			·	,						·	CONDITION	
STREET	TRIB ID				AREA				FUP.	PEAK			GRUSS		RESIDENT	AL FLOW			Length	Size	Slope	Canadity		94 Euli	NOTES
						(Poreone/		UNIS							INIEII	SEMACE	2.00 Ve			D	6	Ocan		70 T CIII	
				(ha)	(ha)	(i ersons/ ha)	(leisons /Unit)			K.	(1143)	INDEX	(ha)	(ha)	0.26 (L/s) 0	0042 (L/s)	43	13	(m)	(mm)	(%)	(1/e)	(m/s)	O(d)/Ocan	
1900 Brook Bood				29.50	20 50	800	, On incy		23600	·뛰 2.58			(114)	(na)	7.67	255 78	0.00	263.45	112.0	(IIII) 525	1.00	420.06	1.00	61 2	EL TT I PE PROPOSED
1099 DIUCK NOAU	ГЭ			23.50	23.00	000			23000	2.50					1.07	200.10	0.00	200.40	112.0	525	1.00	430.00	1.99	01.5	
One dian Trada				4 4 0	4.40	4000			4000	2.05					4.07	67.40	0.00	<u> </u>	50.0	450	0.20	450.40	0.00	40.7	
Canadian Tire Lands	4	EX.MHU90	EX MH 34-82	4.10	4.10	1200			4920	3.20					1.07	07.19	0.00	08.20	59.8	450	0.30	100.10	0.98	43./	EX PIPE OUTSIDE SOUPE OF WORK
Pickering Parkway	13	EX MH 34-82	Prop MH9A	0.25	33 85				28520	2 50				0.00	8 80	299.32	0.00	308 12	49.4	675	0.37	511 31	1 43	60.3	PROPOSED
, ionering i uniti uj				0.20					20020	2.00				0.00	0.00	200.02	0.00	000.12		0.0	0.01				
Subject Site	P1	Prop MH1A	Prop MH2A	1.18	1.18		2.5	630	1575	3.66			0.17	0.17	0.31	24.24	0.35	24.90	20.7	300	0.87	90.20	1.28	27.6	PROPOSED
Subject Site		Prop MH2A	Prop MH3A		1.18				1575	3.66				0.17	0.31	24.24	0.35	24.90	44.7	300	0.95	94.25	1.33	26.4	PROPOSED
Subject Site	P2	Prop MH3A	Prop MH4A	1.23	2.41		2.5	1090	4300	3.31			0.10	0.27	0.63	59.69	0.56	60.88	83.5	300	0.78	85.40	1.21	71.3	PROPOSED
Subject Site		Prop MH4A	Prop MH5A		2.41				4300	3.31				0.27	0.63	59.69	0.56	60.88	47.2	300	1.31	110.68	1.57	55.0	PROPOSED
Subject Site	P3,P4		Prop MH6A	3.11	5.52		2.5	1022	6855	3.12			0.07	0.34	1.44	89.69	0.71	91.84	37.6	300	1.46	116.84	1.65	78.6	PROPOSED
Subject Site	P3,P0		Prop MH8A	2.31	0.03		2.0	12/0	10045	2.90			2.26	2.67	2.09	124.37	0.00	127.31	19.0	450	0.77	200.10	1.57	51.0 79.7	PROPOSED
Subject Site	17,10	Prop MH8A	Prop MH9A	1.45	9.40		2.5	1200	13065	2.04			2.20	2.07	2.40	155.76	5.55	163.78	14.3	450	0.52	203.33	1.29	67.7	PROPOSED
					0.10					2.01				2.01	2.10		0.00				0.72	211.02		••••	
Pickering Parkw ay	13	Prop MH9A	EX MH 34-83	0.25	43.58				41585	2.34				2.67	11.33	408.68	5.55	425.56	41.8	675	0.42	544.76	1.52	78.1	PROPOSED
Pickering Parkw ay	14	EX MH 34-83	EX MH 35-5	0.24	43.82				41585	2.34				2.67	11.39	408.68	5.55	425.62	100.0	675	0.47	576.28	1.61	73.9	PROPOSED
Pickering Parkw ay	15	EX MH 35-5	EX MH 35-6	0.28	44.10				41585	2.34				2.67	11.47	408.68	5.55	425.70	99.8	675	0.48	582.38	1.63	73.1	PROPOSED
																							<u> </u>		
BEECHLAWN DR	7	EX MH018	EX MH 35-6	2.89	2.89	60			173	3.80					0.75	2.77		3.52	59.0	200	0.95	31.97	1.02	11.0	EX
	20			3.65	3 65				672	3.80					0.95	10 73		11.67	38.2	200	0.75	28.40	0.00	/1 1	FY
	20			5.05	5.05				012	5.00					0.35	10.75		11.07	50.2	200	0.75	20.40	0.30	41.1	5
MARSHCOURT DR		EX MH 35-8	EX MH 35-25							0.00					0.00	0.00	0.00	0.00	<del>58.9</del>	<del>25</del> 0	<del>0.41</del>	38.08	0.78	0.0	pipe to remain as cleanout access
																							i – – – – – – – – – – – – – – – – – – –		
ASHFORD DR	8	EX.MH023	SAN MH 35-25	1.93	1.93	60			116	3.80					0.50	1.85		2.35	73.0	200	0.40	20.74	0.66	11.3	EX
																							<u> </u>		
MARSHOOURT DR	9	SAN MH 35-25	SAN MH 35-26	0.29	2.22	60			133	3.80					0.58	2.13	0.00	2.70	83.6	250	0.55	44.10	0.90	6.1	EX
MARSHOURIDR	10	SAN MH 35-20	5AN MH 35-27	0.60	2.82	60			169	3.80					0.73	2.70	0.00	3.43	69.5	250	0.55	44.10	0.90	6.1	EX
MARSHCOURT DR	11	EX MH 032	SAN MH 35-27	17 39	17 39	60			1044	3 79			0.67	0.67	4 52	16 61	1 39	22 52	40.5	250	0 27	30.90	0.63	72.9	FX
			0, 11111100 21	17.00	11.00				1011	0.10			0.07	0.01	1.02	10.01	1.00	22.02	10.0	200	0.27	00.00	0.00	12.0	5
EASEMENT		SAN MH 35-27	SAN MH 35-29		20.21				1213	3.74				0.67	5.25	19.08	1.39	25.72	124.0	375	0.16	70.13	0.63	36.7	outlet to Region Trunk on Notion Rd*
																							<del> </del>		-
Pickering Parkwav	16	EX MH 35-6	EX MH 35-7	0.22	50.86				42430	2.33				2.67	13.22	415.50	5.55	434.28	82.5	750	0.38	686.27	1.55	63.3	PROPOSED
Pickering Parkway	17	EX MH 35-7	EX MH 35-8	0.24	51.10			1	42430	2.33	-			2.67	13.29	415.50	5.55	434.34	80.0	750	0.46	755.06	1.71	57.5	PROPOSED
Pickering Parkw ay	18	EX MH 35-8	EX MH 35-28	0.22	51.32				42430	2.33				2.67	13.34	415.50	5.55	434.40	110.1	750	0.57	840.51	1.90	51.7	outlet to Region Trunk on Notion Rd
Design Criteria as per The Regional Municipality of Durham 'Design Specifications for Sanitary Sewers' Av erage daily per capita flow = 364 L/cap/day (Residential) Av erage daily per capita flow = 180,000 L/GFA hectares/day (commercial&industrial) I = Unit of peak extraneous flow when foundation drains are NOT connected to the storm sewer = 0.26 L/s/Ha 1) MINIMUM VELOCITY = 0.60 m/ 2) MAXIMUM VELOCITY = 3.65 m   I = Unit of peak extraneous flow when foundation drains are NOT connected to the storm sewer = 0.26 L/s/Ha 3) INFILTRATION 0.26 Vs = 22.5 r   IQ(p) = peak population flow (L/s) Q(I) = peak extraneous flow (L/s) Q(d) = peak design flow (L/s) PEAK ING FACTOR (Harmon; Residential) M =1 + 14/(4+(P/1000*0.5)) PEAK POPULATION FLOW, Q (p) = q*P*M / 86400 L / Sec. PEAK EXTRANEOUS FLOW, Q(i) = I*A L / Sec. PIPE ROUGHGNESS, n = 0.013 For Manning's Equation 4) COMMERCIAL 2.08 Vs (local st VNOTES: 1) MINIMUM VELOCITY = 3.65 m							0 m/s 65 m/s 2.5 m3/Ha 5.0 m3/Ha al sewers CLUDES ( PIPE SIZ ACE IND	a/DAY a/DAY (Fou ) 1.04 I/s ( COMMITTE ZE IN mm EX=50% U	undation D trunk sew D DEVEL NLESS O	Drain ers) LOPMENT THERWISE	Popul Housin Single Townh Apartm Housin Single Semi D	ation Density <u>a Type</u> & Semi Detacl ouse nent-2Bdrm <u>a Type</u> Family Detached & Du	by Land U hed plex	58	<u>Density</u> 3.5 P/u 3.0 P/u 2.5 P/u <u>Density</u> 60 pers 100 per	sons/ha sons/ha				0	ODAN-DETECH CONSULTING ENGINEERS				
									*ASSU	ED FLOW F	ROM EA	SEMENT	SEWERA	AND PICK	ERING PARKV	WAY WILL O	UTLET TO	REGION	TRUNK O	N NOTION	IRD				

#### Redeveloped sites (subject site, 1899 Brock Road and surrounding tributaries) sanitary sewer design sheet

#### **APPENDIX C**

FUS Fire Demand Calculations Location of hydrant flow tests Hydrant flow tests

#### **FUS Fire Demand Calculations**

WATER SUPPLY FOR PUBLIC FIRE PROTEC	CTION , FIF		NRITERS	SURVEY						
GUIDE FOR DETERMINATION OF REQUI	RED FIRE FL	LOWS	1							
5 222 6 44										
$F = 220 \times C \times V A$										
F = required fire flow in liters per minute										
C= Coefficient related to the type of cons	truction									
A = the total floor area in square meters										
(excluding basements) in the building										
considered										
	20266 - P	hase 1 (Blr			1	PROJECT.	21 Storey R	ocidential - Mixed Lis	•	
LOCATION:	20200-11	Ildse I (Dic	JCK IJ		-	PROJECT:	31 Storey 10			
OBC OCCUPANCY:		Mixed	Use	1	-	PROJECT No:	21241			
BUILDING FOOT PRINT (m2):	18461								Contents	Charge
# OF STOREYS	31								Non-Combustible	-25%
		1							Limited	-15%
									Combustible	-1370
					<b>_</b>				Combustible	0%
CONSTRUCTION CLASS:		Fire Res	istive						Free Burning	15%
									Rapid Buring	25%
AUTOMATED SPRINKLER PROTECTION		Credit	Total							
NFPA 13 sprinkler standard	yes	30%							Coefficient related to	type of construction
Standard Water Supply	yes	10%	50%						1.5	Wood Frame
Fully Supervised System	yes	10%							1	Ordinary
		50%			<u> </u>				0.8	Non combustible
CONTENTS EACTOR		Limited (	Combusti	blo			-15%		0.6	Fire Resistive
CONTENTS FACTOR.		Lillineu	Jonibusu	Die	1	CHANGE.	-1570		Separation	Charge
EXPOSURE 1 (south)	Distar	ice to Expc	osure Buil	lding (m)		- 45			0-3 m	25%
•			Length	- Height	:	>45	0		3.1 -10 m	20%
EXPOSURE 2 (east)	Distan	ice to Expo	sure Buil	ding (m)	I	21.0	10		10.1 - 20 m	15%
	Distor	- to Ever	Length	- Height	(				20.1 - 30 m	10%
EXPOSURE 3 (west)	Distan	ice to Expu	Sure Bui	ding (m) - Height	ł F	>45	0		30.1 - 45	5% N%
EXPOSURE 4 (north)	Distar	ice to Expc	sure Buil	ding (m)		27.0	10		Firewall	10%
			Length	- Height	2	27.9	10		-	
					T	Total:	20	no more than 75%		
						-				
ARE BUILDINGS CONTIGUOUS:	NO	1								
FIRE RESISTANT BUILDING	Are vertical o	openings and	l exterior ve	ertical com	municat	tions protected with a n	ninimum one	e (1) hr rating?	NO	
CALCULATIONS	C =	0.6		Fire Res	sistive					
	A =	15569	m2	Total					STOREY AREAS m2	
	5 -	16470	1 /min		-				1715	
Pound to Nearest 1000   /min	F -	16000	L/min	must be	_ 20(	00 I /min			1/15	2
		10000	L/						1454	3
CORRECTION FACTORS:	ļ								1454	4
OCCUPANCY		-2400	L/min						1454	5
FIRE FLOW ADJUSTED FOR OCCUPANCY		13600	L/min						1289	6
EXPOSURE CHARGE		2720	L/min						728	9.15/0)
		2720	L/11111						778	16-31 (16)
REQUIRED FIRE FLOW	F =	9520	L/min							
Round to Nearest 1000 L/min	F=	10000	L/min	2642	usgm	1				
	F =	166.67	L/sec							
	-									

#### Location of hydrant flow tests



#### **Fire Flow Testing Report**

000	FLOWMETRIX	rite rit	now resting report		
SLE	PROCESS	Residual Hydrant #	PB557		
	WESTCAN	NFPA Colour Code	BLUE		
		DATE TIME	September 8, 2021 10:30 AM		
		ADDRESS	1972 Notion Rd Pickering, ON		
		SIZE-Inches/mm MATERIAL	12 300 PVC		
RESIDUAL HYDRANT INFO. HYDRANT # N.F.P.A. COLOUR CODE	PB557 BLUE	CONTACT INFO	The Odan/Detech Group Inc. Mark Harris C: (905) 632-3811 ext.122 E: mark@odandetech.com		
STATIC PRESSURE RESIDUAL PRESSURE	psi 74.6psi		Er mankgroundetten teom		
PRESSURE DROP % PRESSURE DROP	<u>14.3</u> psi <u>16.0</u> % psi				
Flow on Water Main At Test Hydrant -	20 psi 3766 USGPM				

FLOW HYDRANT(S) INFO.

HYDRANT	HYD.	OUTLET	NOZZLE	DIFFUSER	DIFFUSER	PITOT	PITOT	FLOW
ASSET	Ħ	DIAMETER	COEFFICIENT	TYPE	COEFFICIENT	READING	FLOW	METER
ID	PORTS	(INCHES)				(psi)	(USGPM)	(USGPM)
pp 207	2	2.5	Round	LPD250	0.90	28.4	804	0
PB390	Z	2.5	Round	LPD250	0.90	28.4	804	0
					Total Flow (USGPM	)	1609	0
					Tradician (LICCOM		10	00



OD G\_FireFlowTestingReport\_Pickering

"If we don't measure it, how do you manage it?"

#### **Fire Flow Testing Report**

000	FLOWMETRIX	The How I		
SLG	INDU-TECH PROCESS	Residual Hydrant #	PB386	
	WESTCAN	NFPA Colour Code	BLUE	
		DATE TIME	5eptember 8, 2021 10:45 AM	
		ADDRESS	1735 Pickering Pkwy Pickering, ON	
		SIZE-inches/mm MATERIAL	12 300 PVC	
RESIDUAL HYDRANT INFO. HYDRANT # N.F.P.A. COLOUR CODE	PB386 BLUE	CONTACT INFO	The Odan/Detech Group Inc. Mark Harris C: (905) 632-3811 ext.122	
STATIC PRESSURE RESIDUAL PRESSURE	83.2 psi 73.8 psi		E: mark@odandetech.com	
PRESSURE DROP % PRESSURE DROP	9.3 psi 11.2 % psi			
Flow on Water Main At Test Hydrant -	20 psi 4283 USGPM			

FLOW HYDRANT(S) INFO.

HYDRANT	HYD.	OUTLET	NOZZLE	DIFFUSER	DIFFUSER	PITOT	PITOT	FLOW
ASSET	#	DIAMETER	COEFFICIENT	TYPE	COEFFICIENT	READING	FLOW	METER
ID	PORTS	(INCHES)				(psi)	(USGPM)	(USGPM)
00200	2	2.5	Round	LPD250	0.90	25.5	762	0
PB309	2	2.5	Round	LPD250	0.90	25.5	762	0
					Total Flow (USGPN	i)	1525	0



OD G\_FireFlowTe stingReport\_Pickering

"If we don't measure it, how do you manage it?"

#### **Fire Flow Testing Report**

000	FLOWMETRIX	The new results		
SIL	PROCESS	Residual Hydrant #	PB888	
	WESTCAN	NFPA Colour Code	BLUE	
		DATE TIME	September 8, 2021 11:00 AM	
		ADDRESS	1785 Pickering Pkwy Pickering, ON	
		SIZE-Inches/mm MATERIAL	12 300 PVC	
RESIDUAL HYDRANT INFO. HYDRANT # N.F.P.A. COLOUR CODE	PB888 BLUE	CONTACT INFO	The Odan/Detech Group Inc. Mark Harris C: (905) 632-3811 ext.122	
STATIC PRESSURE RESIDUAL PRESSURE	80.3 psi 73.7 psi		E: mark@odandetecn.com	
PRESSURE DROP % PRESSURE DROP	6.7 psi 8.3 % psi			
Flow on Water Main At Test Hydrant -	20 psi 4735 USGPM			

FLOW HYDRANT(S) INFO.

HYDRANT	HYD.	OUTLET	NOZZLE	DIFFUSER	DIFFUSER	PITOT	PITOT	FLOW
ASSET	#	DIAMETER	COEFFICIENT	TYPE	COEFFICIENT	READING	FLOW	METER
ID	PORTS	(INCHES)				(psi)	(USGPM)	(USGPM)
00200	1	2.5	Round	LPD250	0.90	22.7	720	0
rbsua	2	2.5	Round	LPD250	0.90	22.7	720	0
					Total Flow (USGPM	)	1439	0
				Total Flow (USGPM) 1439			29	



OD G\_FireFlowTestingReport\_Pickering

"If we don't measure it, how do you manage it?"

#### **APPENDIX D**

XPSWMM models and output upon request Water Balance Calculations

#### Water Balance Calculations

#### CITY OF PICKERING GUIDELINE WATER BALANCE SUMMARY

#### Project: 1755&1805 Pickering Parkway (First Pickering Place) Project No.: 20266

		_
Site Area	7825	m <sup>2</sup>
Rainfall depth required to capture	5	mm
Captured Volume Target (5mm across entire s	39.1	m <sup>3</sup>
(Total Area x Rainfall Depth)		

SURFACE TYPE	SURFACE CAPTURE	AREA	% OF SITE	VOLUME CAPTURE
	(mm)		AREA	(m³)
Green Roof	7	682	8.7	4.8
Landscaped Areas	5	921	11.8	4.6
Roof Area (Drains to Cistern for Reuse)	12.86	2309	29.5	29.7
Asphalt Driveway, Pavers and Concrete (Ground)	0	3913	50.0	0.0
TOTAL		7825	100	39.1

CAPTURED VOLUME BY INTIAL ABSTRACTION (m<sup>3</sup>)

VOLUME OF CISTERN (m<sup>3</sup>) 29.7

CAPTURED VOLUME (m<sup>3</sup>) 39.1

9.4

#### **APPENDIX E**

- Figure 1 Preliminary Site Servicing Plan
- Figure 2 Preliminary Grading Plan
- Figure 3 Post Development Watermain Service
- Figure 4 Post Development Storm Service
- Figure 5a Post Development Sanitary Service
- Figure 5b Post Development Sanitary Service
- Figure 6 Post Sanitary Tributary Area Plan
- Figure 7 Pre Development Storm Tributary Area Plan
- Figure 8 Post Development Storm Tributary Area Plan
- Figure 9 Notion Road Profile
- Figure 10 Pickering Parkway Profile 1/2
- Figure 11 Pickering Parkway Profile 2/2













NG STORM MANHOLE		EXISTING SANITARY MANHOLE		PROPOSED VALVE CHAMBER
OSED STORM MANHOLE	Ó	PROPOSED SANITARY MANHOLE		EXISTING WATER MAIN
NG CATCH BASIN MANHOLE		PROPOSED SANITARY SEWER	· ·	PROPOSED WATER MAIN
OSED CATCH BASIN MANHOLE	$- \rightarrow > -$	EXISTING SANITARY SEWER	•	PROPOSED REDUCER
OSED STORMCEPTOR	-Q-	EXISTING HYDRANT	Ħ	PROPOSED CAP FOR SANITARY, STORM AND/OR WATER AS NOTED
NG CATCH BASIN	<b>+</b>	PROPOSED HYDRANT	~ ~ ^	
OSED CATCH BASIN	$\bowtie$	EXISTING WATER VALVE & BOX	- ~ ~ ~-	DENOTES FIFE TO BE REMOVED
NG STORM SEWER		PROPOSED WATER VALVE & BOX	<del></del>	PROPOSED SLOPE (3:1 OR HIGHER)
OSED STORM SEWER	$\bigotimes$	EXISTING VALVE CHAMBER		
		PROPOSED SIAMESE CONNECTION		PROPERTY LINE

FIGURE 5b
FUNCTIONAL SITE SERVICING PLAN
SANITARY (2 of 2)





![](_page_65_Figure_0.jpeg)

![](_page_66_Figure_0.jpeg)

## PICKERING PARKWAY

## **NOTION ROAD - PROFILE**

## SANITARY IS ON EAST SIDE

## **ORCHARD ROAD**

The Odan/Detech Group Inc. P: (905) 632-3811 F: (905) 632-3363 5230 SOUTH SERVICE ROAD, BURLINGTON, ONTARIO, L7L 5K2

**ODAN-DETECH** CONSULTING ENGINEERS

![](_page_67_Figure_1.jpeg)

# **PICKERING PARKWAY - PROFILE 1of2**

SANITARY IS ON NORTH SIDE

## PIPES TO NOTION ROAD TO BE SIZED AND CONSTRUCTED FOR FULL BUILD OUT OF SUBJECT SITE, 1899 BROCK ROAD AND FUTURE DEVELOPMENTS (PER REGION)

![](_page_67_Figure_5.jpeg)

## **SEE FIGURE 11**

# **PICKERING PARKWAY - PROFILE 2of2**

## **SEE FIGURE 10**

![](_page_68_Figure_2.jpeg)

PR⊡P 82.45m 250mm P∨C SAN @ 0.36%

EX 155.84m 1350mm CONC STM @ 0.33%

EXISTING

SANITARY

EXISTING STORM

49

≥

79. 79.

SANITARY IS ON NORTH SIDE

- PR⊡P 10.40m 250mm PVC SAN @ 1.12%

78.97 78.29

≥≥

## PIPES TO NOTION ROAD TO BE SIZED AND CONSTRUCTED FOR FULL BUILD OUT OF SUBJECT SITE, 1899 BROCK ROAD AND FUTURE DEVELOPMENTS (PER REGION)

PR⊡P 80.09m 250mm P∨C SAN @ 0.46%

![](_page_68_Figure_11.jpeg)

#### The Odan/Detech Group Inc. P: (905) 632-3811 F: (905) 632-3363 5230 SOUTH SERVICE ROAD, BURLINGTON, ONTARIO, L7L 5K2

CONSULTING ENGINEERS